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The crystal structure determinations of trans-dicyano trien cobalt (III) perchlorate and potassium antimony (III) pentachloride and two phase determination techniques based on Patterson deconvolution

Robert Kingsley Wismer
Iowa State University

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AND POTASSIUM ANTIMONY(III) PENTACHLORIDE
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and
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based on Patterson deconvolution

by

Robert Kingsley Wismer

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INTRODUCTION

This thesis describes the crystal structures of two compounds and details two methods for the determination of the phases of structure factors. The crystal structures were undertaken to extend the currently available knowledge of cobalt and antimony complexes.

The cobalt compound was believed by its discoverers to be cis- $\alpha(\text{NC})_2$ trien cobalt(III) perchlorate. Thus, it would have been the sole known mononuclear cobalt complex in which the cyanide group was coordinated to cobalt through the nitrogen atom. The structure that was determined is actually trans- $(\text{CN})_2$ trien cobalt(III) perchlorate and is one of the few examples in which a quadridentate ligand, not restricted by its own structure to be planar, is equatorially coordinated to cobalt.

The second structure described is that of K_2SbCl_5 . The structure of the SbCl_5^- anion has only been determined once previously, in the compound $(\text{NH}_4)_2\text{SbCl}_5$. In that instance, the disagreement between observed and calculated structure factors was such that the uncertainty in bond distances was 0.5 \AA . Structures of antimony halides are known to be very sensitive to the cation present.

The first of the phase determining methods applies the techniques of pseudo heavy atom superposition and then uses space group symmetry to determine atomic

locations in electron density space. All of these operations are performed by a computer program with a minimum of human intervention.

The second phase determining method also uses superposition techniques, to enhance the phase determining properties of a pseudo electron density map which has been computed from origin-defining reflections. The coefficients of the Fourier transform of this modified map are then used to phase those reflections with the largest normalized unitary structure factors. This method greatly simplifies one of the major problems of direct methods, the expansion of the origin-defining set.

THE CRYSTAL AND MOLECULAR STRUCTURE OF TRANS-DICYANO
TRIETHYLENETETRAMINE COBALT(III) PERCHLORATE

Introduction

The bonding mode of cyanide to cobalt has been the subject of considerable controversy in recent years. The energy difference between the cyano and isocyano coordinations is small enough to permit either to occur.¹ However, neutron diffraction studies of cyano-cobalt complexes^{2,3,4} have regularly shown that the cyanide group bonds through carbon. Since it is oftentimes difficult to distinguish between atoms which differ by but one electron by X-ray diffraction, bonding via the carbon has sometimes been assumed.⁵

Kuroda and Gentile⁶ recently have prepared what they characterize as an isocyano cobalt complex, cis- α -isocyano-triethylenetetramine cobalt(III) perchlorate. Their assignment of the isocyano coordination is based on visible and ultraviolet spectroscopy. Because there is some doubt as to the correctness of this assignment,⁷ it was decided to carry out an X-ray structure determination of this compound.

Experimental

A sample of the compound, prepared by the method of Kuroda and Gentile,⁶ was kindly supplied by Dr. James H.

Espenson. Amber-colored crystals were obtained by recrystallization from an aqueous solution. High resolution infrared spectra of the initial sample and of the recrystallized material, both in KBr pellets, were virtually identical, indicating that isomerization had not occurred during solution or recrystallization. Microscopic examination revealed that the crystals have sharply defined faces and are needle-like in appearance with a distorted hexagonal cross section in which alternate sides are of unequal lengths.

Crystals were selected and mounted on a glass fiber with Duco cement thinned with amyl acetate. Preliminary Weissenberg and precession photographs exhibited $2/m$ Laue symmetry, indicating a monoclinic space group. The following systematic absences were observed: $h0\ell$ when $h + \ell = 2n + 1$, and $0k0$ when $k = 2n + 1$. These absences are only consistent with the space group $P2_1/n$. The unit cell parameters at 25°C are $\underline{a} = 9.8544 \pm 0.0015$, $\underline{b} = 22.3529 \pm 0.0045$, $\underline{c} = 6.6766 \pm 0.0020 \text{ \AA}$, and $\beta = 100.85 \pm 0.03^\circ$. These parameters and their standard deviations were obtained by a least squares fit⁸ to the two-theta values of twelve independent reflections whose centers were determined by top-bottom, left-right beam splitting on a previously aligned Hilger-Watts four-circle diffractometer (MoK α radiation, $\lambda = 0.71069 \text{ \AA}$). Any

error in the instrumental zero was eliminated by centering the reflection at both plus two-theta and minus two-theta. A calculated density of 1.62 g/cc for four molecules per unit cell agrees quite well with an observed density of 1.65 ± 0.01 g/cc, which was determined by flotation techniques.

For data collection, a crystal was selected having approximate dimensions 0.1 x 0.1 x 0.9 mm along the a, b, and c crystal axes, respectively, and was mounted such that the c axis coincided with the ϕ axis of the diffractometer. Data were collected at room temperature using a Hilger-Watts four-circle diffractometer interfaced to an SDS 910 computer in a real time mode, equipped with a scintillation counter, and using Zr-filtered MoK α radiation. Within a two-theta sphere of 60° ($\sin\theta/\lambda = 0.704 \text{ \AA}^{-1}$) all data in the hk^l and $\bar{h}k^l$ octants were recorded using the θ - 2θ scan technique with a take-off angle of 5.5°. Symmetric scan ranges of 1.2° in 2θ at low two-theta values to 2.0° at large two-theta values were used. Stationary-crystal, stationary-counter background counts of half the scan time were taken at the beginning and end of each scan. A counting rate of 0.4096 seconds per step of 0.01° in θ was employed. A total of 5081 reflections were measured in this way.

As a general check on electronic and crystal stability, the intensities of three standard reflections were remeasured periodically during the data collection period. These reflections did not vary to any significant degree during the entire period of data collection.

Based on a linear absorption coefficient of $\mu = 14.982 \text{ cm}^{-1}$, the maximum and minimum transmission factors⁹ were 87.86% and 85.96% respectively, and no absorption correction was deemed necessary.

The intensity data were corrected for Lorentz-polarization effects. The estimated error in each intensity was calculated by

$$\sigma_I^2 = C_T + C_B + (0.03 C_T)^2 + (0.03 C_B)^2$$

where C_T and C_B are the total count and the background count, respectively. The factor 0.03 represents an estimate of non-statistical errors. The estimated deviations in the structure factors were calculated by the finite difference method.¹⁰ Of the 4678 independent reflections, 3314 were considered observed ($> 3\sigma_F$).

Solution and Refinement

The positions of the cobalt and chlorine atoms were obtained from analysis of a sharpened Patterson function.¹¹ The remaining non-hydrogen atoms were found by successive structure factor¹² and electron density map calcula-

tions.^{13,14} These atomic positions were then refined by a full matrix least squares procedure,¹² minimizing the function $\sum w (|F_o| - |F_c|)^2$, where $w = 1/\sigma_F^2$, to a conventional discrepancy factor of $R = \sum ||F_o| - |F_c|| / \sum |F_o| = 0.170$. The scattering factors used were those of Hanson et al.¹⁵ with the cobalt and chlorine scattering factors modified for the real and imaginary parts of anomalous dispersion.¹⁶

An electron density difference map verified that all the non-hydrogen atoms had been accounted for, but indicated that some anisotropic motion, particularly of the cobalt and chlorine atoms, was present. Accordingly, anisotropic refinement was begun and after six cycles of refinement, values of R and $R (= \sum w (|F_o| - |F_c|)^2 / \sum w |F_o|^2)^{1/2}$ of 0.154 and 0.169, respectively, were obtained. The positions of the hydrogens bonded to carbons in the triethylenetetramine ligand were calculated with an H-C-C angle of 109.5° and a C-H distance of 1.07 \AA . The hydrogen atoms were assigned isotropic thermal parameters of 3.0 \AA^2 . Two cycles of refinement with anisotropic thermal parameters for all non-hydrogen atoms, varying only the positional and thermal parameters of the non-hydrogen atoms and the overall scale factor, followed by a recalculation of the hydrogen atom positions and two further cycles of least squares refinement, yielded values for R and wR of 0.123

and 0.156, respectively.

A final electron density difference map showed no peaks greater than $1.2 \text{ e}/\text{\AA}^3$. A final statistical analysis of the F_o and F_c values as a function of the scattering angle and magnitude of F_o revealed no unusual trends and suggests that the relative weighting scheme used is a reasonable one.

The bonding orientation of the two cyanide groups was determined after the final least squares refinement. The atom multipliers of the two cyanide group atoms were allowed to vary under two sets of conditions. In the first of these, carbon scattering factors were assigned to C(7) and C(8) and nitrogen scattering factors were assigned to N(5) and N(6). In the second instance, the scattering factor assignments were reversed. All four atom multipliers were initially set at a value of 1.00. The results of these refinements are shown in Table I and clearly indicate the correct assignments.

The final positional and thermal parameters for the non-hydrogen atoms are listed in Table II. The standard deviations were calculated from the inverse matrix of the final least squares refinement cycle. The calculated hydrogen atom positions are listed in Table III. Bond

Table I. Determination of the bonding mode of cyanide in
trans-(CN)₂ trien Co^{III}ClO₄

Atom	Assigned Scattering Factor Table	Atom Actual	Multiplier		R	ωR
			Co-C-N	Co-N-C		
C(7)	Carbon	1.033	1.0	1.17		
C(8)	Carbon	1.034	1.0	1.17		
N(5)	Nitrogen	1.026	1.0	0.86		
N(6)	Nitrogen	1.046	1.0	0.86	12.4	15.8
C(7)	Nitrogen	0.823	0.86	1.0		
C(8)	Nitrogen	0.825	0.86	1.0		
N(5)	Carbon	1.293	1.17	1.0		
N(6)	Carbon	1.314	1.17	1.0	12.4	15.8

Table II

Final positional and anisotropic thermal parameters of non-hydrogen atoms in trans-(NC)₂-trien: Co^{III}ClO₄^{a, b}

Atom	x	y	z	10 ⁴ β ₁₁	10 ⁴ β ₂₂	10 ⁴ β ₃₃	10 ⁴ β ₁₂	10 ⁴ β ₁₃	10 ⁴ β ₂₃
Co	0.6629(1)	0.3488(1)	0.6552(2)	55.9(1.4)	9.2(0.2)	169.9(3.6)	1.1(0.5)	13.9(1.6)	0.7(0.9)
Cl	0.6616(3)	0.1289(1)	0.6466(6)	79.7(3.0)	15.6(0.6)	306.3(9.7)	3.6(1.1)	12.7(4.3)	6.1(2.2)
O(1)	0.6601(9)	0.0863(4)	0.4868(15)	139(12)	21(2)	360(32)	10(4)	-26(16)	11(7)
O(2)	0.5498(9)	0.1700(4)	0.5928(16)	121(12)	30(2)	486(39)	32(4)	-79(17)	43(8)
O(3)	0.7893(8)	0.1635(4)	0.6748(15)	92(10)	26(2)	386(32)	-5(4)	-7(14)	13(7)
O(4)	0.6586(11)	0.0988(5)	0.8283(16)	204(17)	34(3)	333(33)	-2(5.6)	90(19)	-3(9)
N(1)	0.4727(8)	0.3159(4)	0.5898(14)	69(9)	14(2)	198(24)	-9(3)	2(12)	10(6)
N(2)	0.5927(8)	0.4122(3)	0.8075(12)	77(9)	11(2)	148(21)	3(3)	11(11)	4(5)
N(3)	0.8378(8)	0.3891(4)	0.7368(15)	66(9)	14(2)	224(26)	-4(3)	23(13)	-9(6)
N(4)	0.7579(9)	0.2898(4)	0.5051(13)	97(11)	14(2)	197(25)	8(4)	39(13)	7(6)
C(7)	0.6226(10)	0.3942(5)	0.4078(12)	63(11)	12(2)	205(30)	3(4)	17(15)	-8(6.7)
C(8)	0.6997(10)	0.3013(4)	0.8952(13)	63(11)	9(2)	250(33)	-7(3.5)	31(15)	-7(7)
C(1)	0.3914(11)	0.3494(6)	0.7122(20)	77(12)	22(3)	274(36)	-7(5)	15(17)	-5(9)
C(2)	0.4392(11)	0.4144(5)	0.7393(20)	62(11)	20(3)	313(39)	10(4)	39(17)	15(9)
C(3)	0.6694(12)	0.4679(5)	0.7878(19)	93(13)	12(2)	280(37)	-4(4)	3(17)	-11(8)
C(4)	0.8173(13)	0.4546(5)	0.7531(24)	118(17)	16(3)	388(47)	-7(5)	11(22)	-19(9)
C(5)	0.9274(12)	0.3720(6)	0.6003(21)	81(13)	26(3)	289(40)	-5(5)	42(19)	-15(10)
C(6)	0.9102(13)	0.3046(6)	0.5589(23)	105(16)	26(3)	407(50)	13(6)	36(23)	14(11)
N(5)	0.6027(11)	0.4174(5)	0.2486(19)	116(13)	19(2)	349(38)	3(4)	27(18)	9(8)
N(6)	0.7204(10)	0.2762(4)	1.0540(15)	115(12)	16(2)	230(28)	3(4)	28(15)	5(7)

^a In this and subsequent tables, numbers in parentheses represent standard deviations in the least significant digits.^b Anisotropic thermal parameters are defined by: $T = \exp[-(h^2\beta_{11} + k^2\beta_{22} + l^2\beta_{33} + 2hk\beta_{12} + 2kl\beta_{23} + 2hl\beta_{13})]$.

Table III. Calculated hydrogen atomic positions in trans-
(CN)₂ trien Co^{III}ClO₄

Atom	x	y	z
H(AC1)	0.4041	0.3289	0.8624
H(BC1)	0.2834	0.3479	0.6404
H(AC2)	0.3934	0.4374	0.8519
H(BC2)	0.4113	0.4386	0.5960
H(AC3)	0.6762	0.4947	0.9921
H(BC3)	0.6135	0.4932	0.6569
H(AC4)	0.8303	0.4765	0.6143
H(BC4)	0.8906	0.4724	0.8798
H(AC5)	1.0339	0.3827	0.6673
H(BC5)	0.8990	0.3961	0.4566
H(AC6)	0.9606	0.2912	0.4366
H(BC6)	0.9593	0.2799	0.6960

lengths and bond angles, and significant non-bonded distances are listed in Tables IV and V, respectively, along with their standard deviations.¹⁷ The final values of the observed and calculated structure factors are listed in Table VI.

Shortly after the data had been collected and the crystal removed from the diffractometer, the instrument was found to be slightly misaligned. Thus, the data are somewhat poorer than might be expected. However, since all the stereochemical features of interest were well determined and the electron density difference map was rather featureless, the data were not retaken.

Description of the Structure

The results clearly indicate that the bonding of cyanide to the cobalt is through the carbon and not the nitrogen, and that these groups are trans and not cis to one another, contrary to the predictions of Kuroda and Gentile.⁶ Hence, the compound is trans-dicyanotriethylene-tetramine cobalt(III) perchlorate, and is illustrated in Figure 1.¹⁸ This configuration has been anticipated by Konya, Nishikawa, and Shibita⁷ on the basis of spectroscopic examination of similar compounds. The trans configuration is also consistent with an exceedingly sharp band for the C-N stretching frequency at 2145 cm^{-1} , with no evidence of splitting.

Table IV. Selected bond distances and angles in angstroms and degrees for cis-(CN)₂ trien Co^{III}ClO₄

Cl-O(1)	1.427(9)	C(8)-N(6)	1.180(13)
Cl-O(2)	1.424(8)	N(1)-C(1)	1.462(15)
Cl-O(3)	1.456(9)	N(2)-C(2)	1.488(12)
Cl-O(4)	1.392(10)	N(2)-C(3)	1.476(13)
Co-N(1)	1.978(8)	N(3)-C(4)	1.484(14)
Co-N(2)	1.951(8)	N(3)-C(5)	1.444(15)
Co-N(3)	1.922(8)	N(4)-C(6)	1.506(15)
Co-N(4)	2.001(8)	C(1)-C(2)	1.527(16)
Co-C(7)	1.909(12)	C(3)-C(4)	1.551(17)
Co-C(8)	1.894(12)	C(5)-C(6)	1.536(18)
C(7)-N(5)	1.161(14)		
O(1)-Cl-O(2)	110.7(6)	N(4)-Co-C(8)	91.5(4)
O(1)-Cl-O(3)	109.1(6)	C(7)-Co-C(8)	177.9(4)
O(1)-Cl-O(4)	109.3(6)	Co-N(1)-C(1)	106.7(6)
O(2)-Cl-O(3)	107.1(6)	Co-N(2)-C(2)	108.1(7)
O(2)-Cl-O(4)	112.3(7)	Co-N(2)-C(3)	108.9(7)
O(3)-Cl-O(4)	108.4(6)	Co-N(3)-C(4)	110.8(7)
N(1)-Co-N(2)	88.0(4)	Co-N(3)-C(5)	109.0(7)
N(1)-Co-N(3)	172.5(4)	Co-N(4)-C(6)	106.3(7)
N(1)-Co-N(4)	99.4(4)	Co-C(7)-N(5)	173.7(10)
N(1)-Co-C(7)	89.2(4)	Co-C(8)-N(6)	174.1(9)

Table IV (Continued)

N(1)-Co-C(8)	89.2(4)	N(1)-C(1)-C(2)	111.3(9)
N(2)-Co-N(3)	84.5(4)	N(2)-C(2)-C(1)	105.9(8)
N(2)-Co-N(4)	172.6(4)	N(2)-C(3)-C(4)	111.4(8)
N(2)-Co-C(7)	91.8(4)	N(3)-C(4)-C(3)	110.2(9)
N(2)-Co-C(8)	89.6(4)	N(3)-C(5)-C(6)	108.3(10)
N(3)-Co-N(4)	88.1(4)	N(4)-C(6)-C(5)	109.1(9)
N(3)-Co-C(7)	90.7(4)	C(2)-N(2)-C(3)	116.8(8)
N(3)-Co-C(8)	91.0(4)	C(4)-N(3)-C(5)	114.5(10)
N(4)-Co-C(7)	87.3(4)		

Table V. Significant non-bonded distances in trans-(CN)₂
trien Co^{III}ClO₄^a

C(7)-H(BC3)	2.870(10)
C(7)-H(AC4)	2.884(10)
C(8)-O(2)	2.694(13)
C(8)-O(3)	3.601(13)
N(4)-O(3)	3.034(12)
O(1)-H(AC5)'	2.34(1)
O(4)-H(BC1)'	2.49(1)

^a Primed atoms indicate atoms in another molecule.

Table VI. Observed and calculated structure factors

Table VI. Observed and calculated structure factors. The table contains multiple columns of data, including Miller indices (h, k, l), observed structure factors (F_o), and calculated structure factors (F_c). The data is organized into several sections, likely corresponding to different reflections or symmetry-equivalent points. The observed values are typically integers, while the calculated values are often decimal fractions. The table is very dense and spans most of the page.

Table VI. (Continued)

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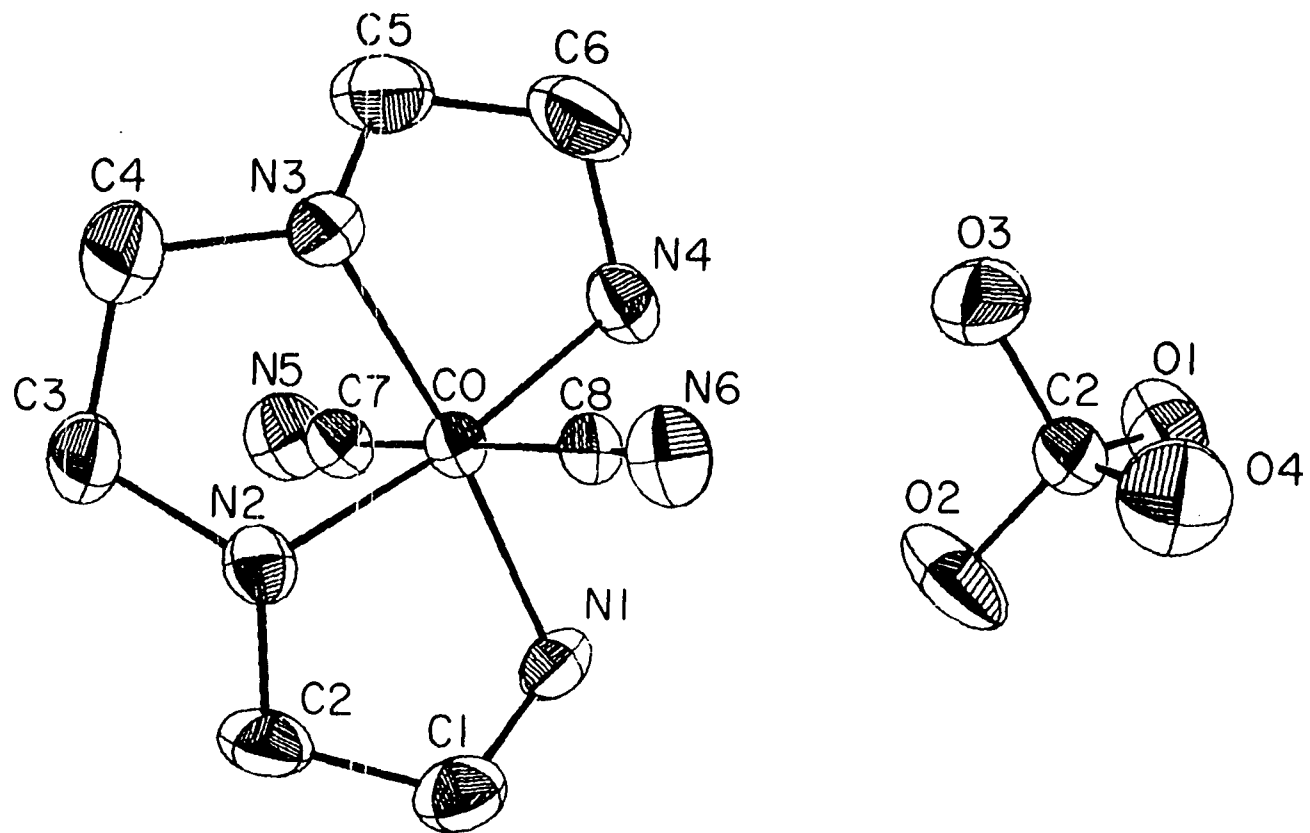


Figure 1. A formula unit of trans-cyano triethylenetetramine cobalt(III) perchlorate

The cyanide groups are within a degree of being perpendicular to the nitrogens of the trien ligand (Table IV), and the variations from an ideal octahedral configuration displayed by the N-Co-N angles appear to simply reflect the restrictions imposed by the quadridentate ligand (Figure 2). This trien ligand coordinated to cobalt in a cis configuration has been investigated by Freeman and Maxwell,¹⁹ and Dwyler and Maxwell;²⁰ their results have been used as the basis of many of the comparisons which follow.

The N(1)-Co-N(2) and N(3)-Co-N(4) angles of 88.0 and 88.1° are reasonable and consistent with similar results obtained in other investigations of the trien ligand. A slight compression of the Co-N(2)-C(3)-C(4)-N(3) ring due to the equatorial coordination of the ligand adequately explains the somewhat small value of 84.5° for the N(2)-Co-N(3) angle. Hydrogen-hydrogen repulsions would be expected to produce an increase in the N(1)-Co-N(4) angle compared to the nominal 90°, and the 99° angle found is quite reasonable. A similar result was obtained during the investigation of a cobalt compound containing a homologous ligand.²¹ The bond angles within the trien ligand, with the exception of the C-N-C angles, do not differ from the expected tetrahedral angles by more than three standard deviations. In addition, they fall within two standard deviations of the range of values of 108.4°

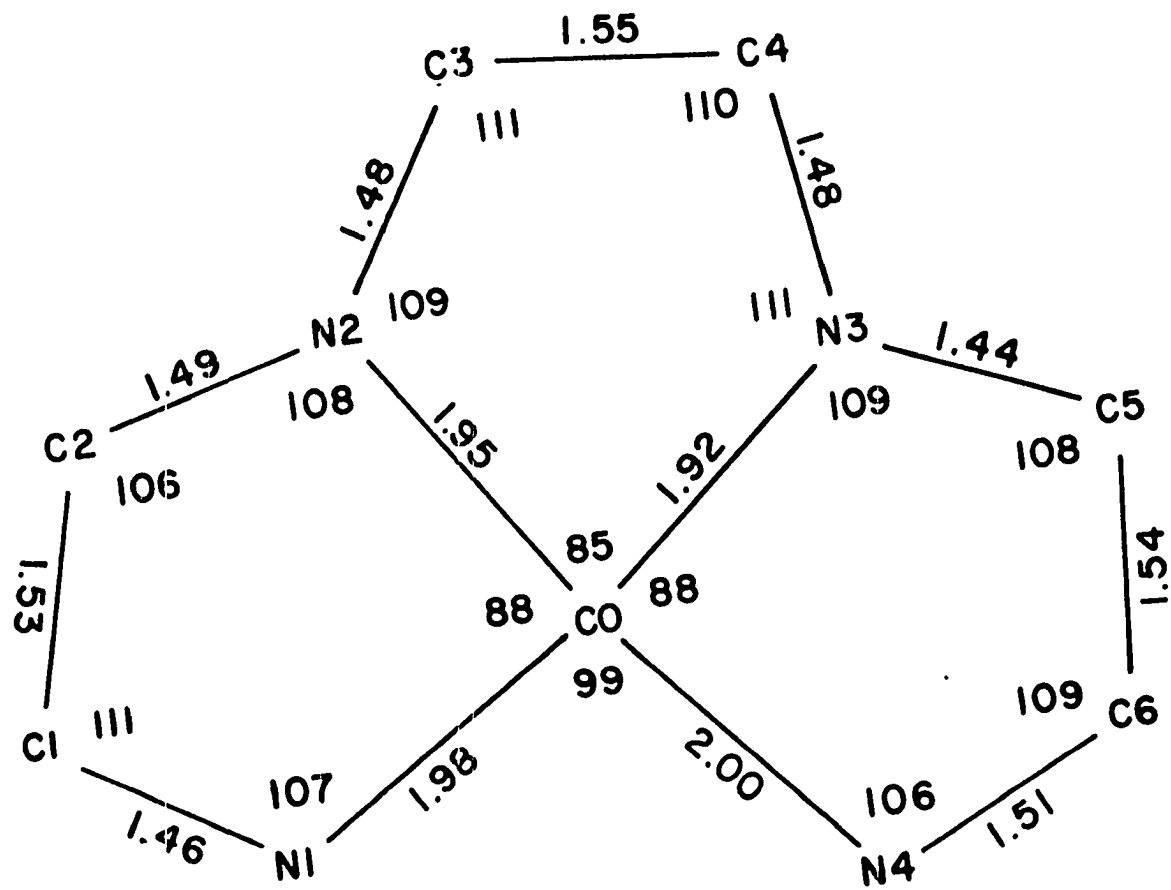


Figure 2. Bond distances and angles within the trien ligand

to 112.3° for Co-N-C bonds, and of 105.2° to 111.4° for N-C-C bonds reported by other investigators of this ligand. The C-N-C bond angles of 116.8° and 114.6° are also reasonable in view of the fact that the Co-N-C angles are, on the average, somewhat less than tetrahedral. These C-N-C angles also agree within three standard deviations with other results obtained in investigations of this ligand.

The bond distances within the trien ligand range from 1.92 to 2.00 Å for Co-N bonds, from 1.44 to 1.51 Å for N-C bonds, and from 1.53 to 1.55 Å for C-C bonds, with average values of 1.96, 1.48, and 1.54 Å, respectively. These distances in no instance differ significantly from previously reported values for other compounds involving the trien ligand coordinated to cobalt.

The four trien nitrogens and the cobalt atom all fall within 0.01 Å of the least squares plane. The three five-membered rings formed by the quadridentate ligand and the cobalt atom are not planar, however, as the carbon atoms are located above and below the N-Co-N planes. Nonetheless, all of the atoms in the trien ligand fall within 0.37 Å of a least squares plane.

As has been described above, the coordination of the cyanide groups to the cobalt is clearly through the carbon. The Co-C average bond distance of 1.90 Å is in good

agreement with previously published values. The average C-N distance of 1.17 \AA also agrees quite well with the range of previously reported values, 1.15 to 1.18 \AA .^{2,22-24} The fact that no part of the chain N(6)-C(8)-Co-C(7)-N(5) is linear, with bond angles of N(6)-C(8)-Co, C(8)-Co-C(7), and Co-C(7)-N(5) of 174.1 , 177.9 , and 173.7° , respectively, is somewhat unusual but not surprising. Curry and Runciman² have already observed such a phenomenon. Much of this can be attributed to steric effects both inside the moiety and between moieties (Figure 3). Significant non-bonded distances are given in Table V.

The Cl-O bond distances in the perchlorate group average 1.42 \AA and the angles average 109.5° . The relatively large thermal parameters, possibly due to spatial as well as temporal disorder probably account for the large individual deviations from the average values. However, these average values agree reasonably well with previously published values for this anion.²¹ A weak hydrogen bond is possible between N(4) and O(3), which are 3.03 \AA apart. Such a hydrogen bond would help stabilize the perchlorate group.

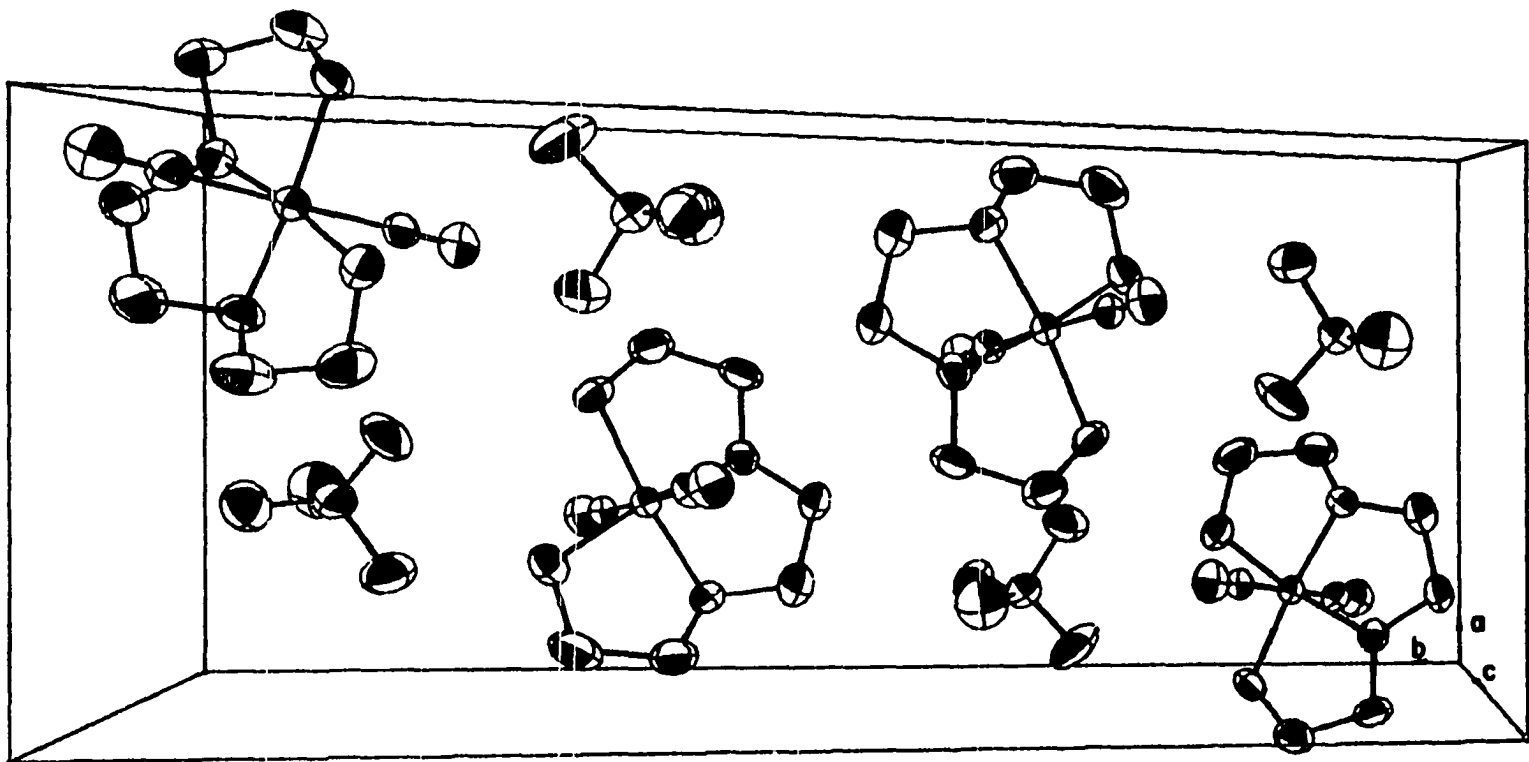


Figure 3. Unit cell showing packing of trans-cyano triethylenetetramine cobalt(III) perchlorate

THE STRUCTURE OF POTASSIUM
ANTIMONY(III) PENTACHLORIDE

Introduction

Structural investigations of antimony halide complexes have been actively pursued in this laboratory during recent years, beginning with the work of Lawton and Jacobson.²⁵ The structures of species containing antimony(III) are of particular interest because of questions concerning the stereochemical role of the lone pair of electrons.

Only a very few antimony(III) chloride structures have been reported in the literature. SbCl_3 exhibits a trigonal pyramid structure with antimony at the apex,²⁶ while in $(\text{NH}_4)_2\text{SbCl}_5$ the chlorine atoms are arranged in a square pyramidal coordination geometry around the antimony.²⁷ In $[\text{C}_5\text{H}_5\text{NH}][\text{Sb}^{\text{III}}\text{Cl}_4]$, the halogen configuration around the antimony can be described as tetragonally distorted octahedral with two of the equatorial atoms removed,²⁸ and SbCl_6^{3-} forms perfect octahedra in $\text{Co}(\text{NH}_3)_6\text{SbCl}_6$.²⁹

Because of the relatively poor determination ($R = 0.24$) of the structure of $(\text{NH}_4)_2\text{SbCl}_5$ and because of the seeming variety of structural geometries possible for antimony(III), it was decided to undertake a structure determination of K_2SbCl_5 .

Experimental

A sample of K_2SbCl_5 was kindly supplied by Dr. Donald Macalady, who prepared the compound in the following manner: Two solutions, one of $SbCl_3$ in 3N HCl and one of KCl in 3N HCl, were combined so that the molar ratio of potassium to antimony in the resulting solution was 5:7. This solution was allowed to stand, and crystals formed by slow evaporation. Microscopic examination revealed many different crystal morphologies. Thin plates appeared to be the basic unit of all these morphologies, however.

A crystal was cut from one of these plates and mounted on the end of a glass fiber with Duco cement thinned with amyl acetate. Preliminary Weissenberg and precession photographs exhibited 2/m Laue symmetry, indicating a monoclinic space group. The following systematic absences were observed: $h0i$ when $i = 2n + 1$, and $0k0$ when $k = 2n + 1$. These absences are only consistent with the space group $P2_1/c$. The unit cell parameters at 25°C are $\underline{a} = 8.8686 \pm 0.0007$, $\underline{b} = 12.4577 \pm 0.0013$, $\underline{c} = 8.9280 \pm 0.0013$ Å and $\beta = 110.512 \pm 0.011^\circ$. These parameters and their standard deviations were obtained by a least squares fit⁸ to the 2θ values of sixteen independent reflections whose centers were determined by left-right, top-bottom beam splitting on a previously aligned four-circle diffractometer (MoK α radiation, $\lambda = 0.71069$ Å). A calculated

density of 2.711 g/cc for four molecules per unit cell agrees quite well with an observed density of 2.72 ± 0.01 g/cc, determined by flotation techniques.

For data collection the crystal described above, measuring approximately 0.2 mm along each of the crystal axes, was mounted so that the c axis coincided with the ϕ axis of the diffractometer. Data were collected at room temperature using an automated four-circle diffractometer designed and built in the Ames Laboratory. The upper full circle was purchased from STOE and is equipped with encoders (Baldwin Optical) and drive motors. The design of the base allows the encoders to be directly connected to the main θ and 2θ shafts, using solid and hollow shaft encoders, respectively. The diffractometer is interfaced to a PDP-15 computer in a real time mode and is equipped with a scintillation counter. Zirconium-filtered $\text{MoK}\alpha$ radiation was used for the data collection. A scan rate of 0.1 second per step of 0.01° in θ was employed with a variable scan range of 35 steps plus 1 step per degree theta. Stationary-crystal, stationary-counter background counts of a quarter of the scan time were taken at the beginning and end of each scan. Before the scan was made a peak height measurement was used to determine if the reflection was observed. To be scanned, the reflection had to exceed the background by

more than six counts. If the reflection met this criterion, the ω setting was then adjusted slightly, if necessary, to maximize the peak height. Within a two-theta sphere of 50° ($\sin\theta/\lambda = 0.595 \text{ \AA}^{-1}$), all data in the hkl and $\bar{h}k\bar{l}$ octants were measured in this manner, using a take-off angle of 4.5° . Of the 1750 reflections examined, 1614 met the peak height criterion and were scanned.

As a general check on electronic and crystal stability, the intensities of three standard reflections were remeasured every twenty-five reflections. These reflections did not vary to any significant degree during the entire period of data collection.

The intensity data were corrected for Lorentz-polarization effects and for effects due to absorption. An absorption correction was made using the Tompa-Alcock absorption correction program^{30,31} using a linear absorption coefficient of $\mu = 52.28 \text{ cm}^{-1}$. The maximum and minimum transmission factors were 43.95% and 35.98%, respectively. The estimated error in each intensity was calculated by

$$\sigma_I^2 = C_T + 2C_B + (0.03 C_T)^2 + (0.03 C_B)^2 + (0.03 C_I)^2 T_a^2,$$

where C_T , C_B , C_I , and T_a are the total count, the

background count, the net count, and the transmission factor, respectively, and the factor 0.03 represents an estimate of non-statistical errors. The estimated deviations in the structure factors were calculated by the finite difference method.¹⁰ Of the 1614 independent reflections, 1543 were considered observed ($> 2.0\sigma_F$).

Solution and Refinement

The position of the antimony atom was obtained from analysis of a sharpened three-dimensional Patterson function.¹¹ The remaining atoms were found by successive structure factor¹² and electron density map calculations.¹⁴ These atomic positions were refined by a full matrix least squares procedure,¹² minimizing the function $\sum \omega (|F_o| - |F_c|)^2$, where $\omega = 1/\sigma_F^2$, to a conventional discrepancy factor of $R = 0.169$. The scattering factors used were those of Hanson *et al.*,¹⁵ modified for the real and imaginary parts of anomalous dispersion.¹⁶

An electron density difference map verified that all the atoms had been accounted for, but indicated that some anisotropic motion, particularly of the antimony, was present. Accordingly, anisotropic refinement was begun and after four cycles of refinement, values of R and ωR of 0.054 and 0.078, respectively, were obtained.

A final electron density difference map showed no peaks greater than $0.9 \text{ e}/\text{\AA}^3$. A final statistical analysis of $\overline{w\Delta^2}$, where $\Delta = (|F_o| - |F_c|)$, as a function of the scattering angle and magnitude of F_o revealed no unusual trends and suggests that the relative weighting scheme used is a reasonable one.

The final positional and thermal parameters are listed in Table VII. The standard deviations were calculated from the inverse matrix of the final least squares cycle. Bond lengths, bond angles, and significant non-bonded distances¹⁷ are listed in Table VIII. The final values of the observed and calculated structure factors are listed in Table IX.

Description and Discussion

The configuration of SbCl_5^- in K_2SbCl_5 is essentially that of a square pyramid which has been distorted by interionic and packing forces. The inversion-related anions are packed approximately base to base, as depicted in Figure 4.¹⁸ The axial antimony-chlorine bond length is 2.385 \AA , in good agreement with the axial distance in $(\text{NH}_4)_2\text{SbCl}_5$ (2.36 \AA),²⁷ the shorter distance (2.38 \AA) in $[\text{C}_5\text{H}_5\text{NH}][\text{Sb}^{\text{III}}\text{Cl}_4]$,²⁸ and only slightly longer than the distance (2.32 \AA) in SbCl_3 .²⁶

Table VII. Final atomic coordinates and thermal parameters ($\times 10^4$) for K_2SbCl_5 ^a

Atom	x	y	z	β_{11}	β_{22}	β_{33}	β_{12}	β_{13}	β_{23}
Sb	0.1836(1)	-0.0068(1)	0.2025(1)	75(1)	42(1)	80(1)	-2(.4)	20(.8)	-3(.4)
Cl(1)	0.2414(3)	0.0959(2)	0.0510(3)	141(4)	55(2)	98(3)	-3(2)	47(3)	3(2)
Cl(2)	-0.0097(3)	0.1519(2)	0.2070(3)	90(3)	51(2)	160(4)	6(2)	47(3)	2(2)
Cl(3)	0.4157(3)	-0.1400(2)	0.2121(3)	143(4)	68(2)	115(4)	35(2)	41(3)	.8(2)
Cl(4)	0.3885(3)	0.1137(2)	0.3563(3)	89(3)	61(2)	99(3)	-17(2)	26(3)	-9(2)
Cl(5)	0.1706(3)	-0.0770(2)	0.4611(3)	118(4)	67(2)	100(3)	-11(2)	40(3)	16(2)
K(1)	0.1853(3)	0.1746(2)	0.5939(3)	135(3)	56(1)	112(3)	2(2)	52(3)	-1(2)
K(2)	0.3742(3)	-0.1285(2)	0.8452(3)	106(3)	94(2)	129(4)	5(2)	43(3)	-24(2)

^a Anisotropic thermal parameters are defined by:

$$T = \exp \left(-h^2\beta_{11} - k^2\beta_{22} - l^2\beta_{33} - hk\beta_{12} - hl\beta_{13} - kl\beta_{23} \right) .$$

Table VIII. Bond lengths, bond angles, and significant non-bonded distances in K_2SbCl_5 ^a

Sb-Cl(1)	2.799(2)	Sb-Cl(2)	2.625(2)
Sb-Cl(3)	2.622(2)	Sb-Cl(4)	2.385(2)
Sb-Cl(5)	2.509(2)		
Cl(4)-Sb-Cl(1)	81.92(7)	Cl(4)-Sb-Cl(2)	83.54(8)
Cl(4)-Sb-Cl(3)	87.06(8)	Cl(4)-Sb-Cl(5)	87.77(8)
Cl(1)-Sb-Cl(2)	88.50(7)	Cl(2)-Sb-Cl(5)	90.43(8)
Cl(5)-Sb-Cl(3)	92.19(3)	Cl(3)-Sb-Cl(1)	87.22(8)
Cl(1)-Sb-Cl(5)	169.69(8)	Cl(2)-Sb-Cl(3)	170.13(8)
Sb-Sb'	3.932(1)	Sb-Cl(2)'	3.881(3)
Cl(1)-Sb'	3.701(2)	Cl(1)-Cl(2)'	3.699(3)
Cl(2)-Cl(5) _i	3.768(3)	Cl(1)-Cl(3) _{ii}	3.832(4)
Cl(1)-K(1) _{iii}	3.187(3)	Cl(1)-K(2) _{iii}	3.290(3)
Cl(2)-K(2) _{iii}	3.168(3)	Cl(1)-K(1) _{iv}	3.247(3)
Cl(2)-K(1) _{iv}	3.147(3)	Cl(3)-K(2) _v	3.190(4)
Cl(2)-K(1)	3.289(3)	Cl(4)-K(1)	3.317(3)

^a Primed atoms are those related by the center of inversion, as in Figure 4. Other symmetry operations referred to are: (i) $-x, \frac{1}{2}+y, -z$; (ii) $x, y, z-1$; (iii) $x, \frac{1}{2}-y, z-1$; (iv) $x, -\frac{1}{2}-y, z-1$; (v) $1-x, -y, -z$.

Table IX. Observed and calculated structure factors

Table IX contains multiple columns of numerical data, organized into several distinct sections. Each section begins with a header row containing labels such as 'h', 'k', 'l', 'F_o', and 'F_c'. The data rows consist of integers, some of which are enclosed in small boxes. The table is densely packed with these numerical entries, representing the observed and calculated structure factors for various crystallographic reflections.

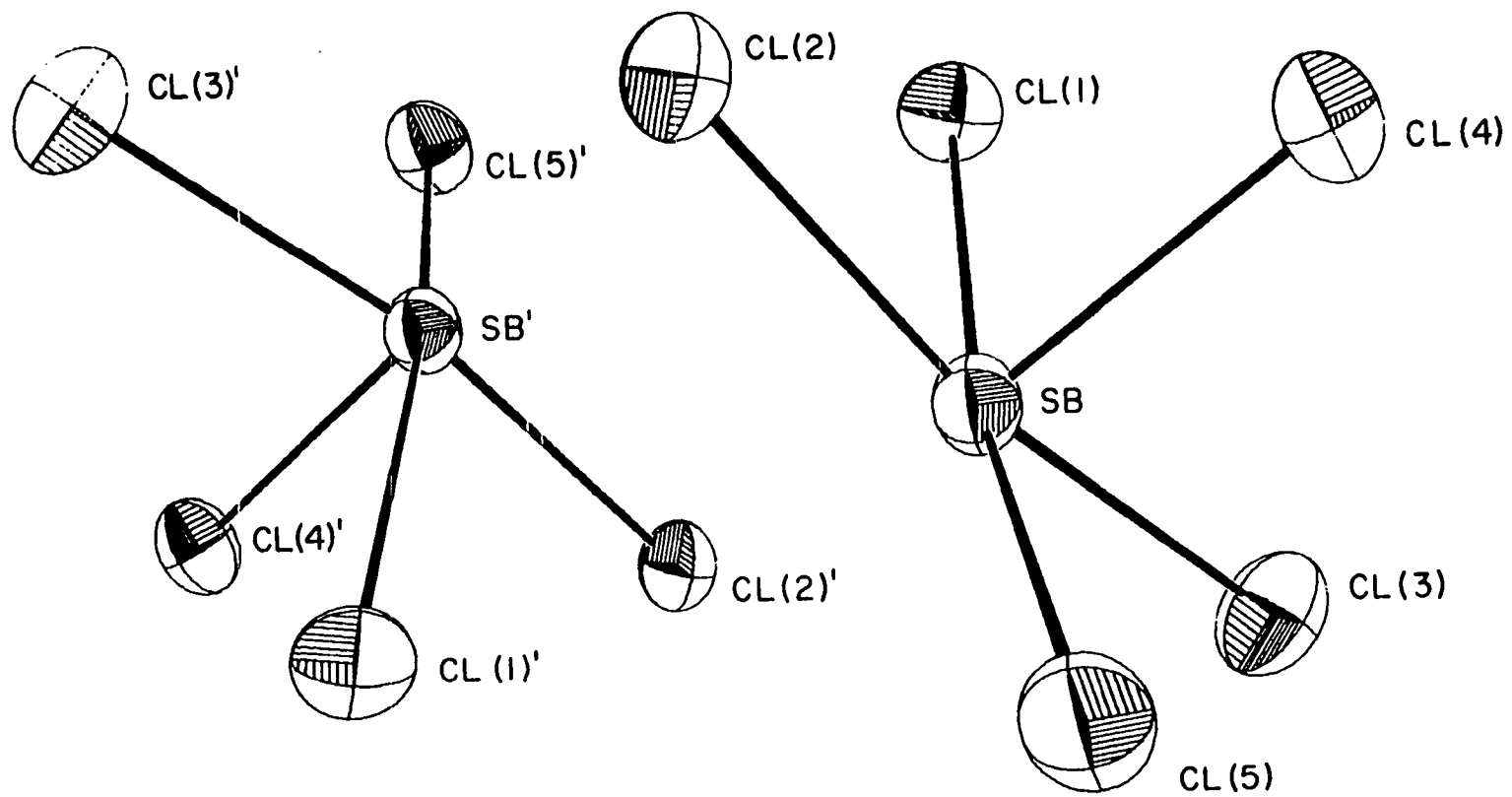


Figure 4. Two inversion-related SbCl_5^- anions

The antimony-chlorine bond distances in the base are all considerably longer than the axial distance. Two of these distances are almost identical (2.622, 2.625 Å) and involve chlorines trans to each other. The other pair of chlorines form bonds of 2.799 and 2.509 Å length, with an average of 2.654 Å. In $(\text{NH}_4)_2\text{SbCl}_5$ all basal antimony-chlorine bonds were found to be essentially of equal length (2.62 Å average) while in $[\text{C}_5\text{H}_5\text{NH}][\text{SbCl}_4]$ the corresponding bond length for chlorines trans to one another is 2.63 Å.

In the present study, the lengthening of the Sb-Cl(1) distance to 2.799 Å appears to be due to electrostatic repulsions and packing effects, as it is this chlorine that is involved in the closest non-bonded contacts; significant non-bonded distances are given in Table VIII. An antimony atom is only 3.701 Å from Cl(1), whereas the sum of the van der Waal's radii is 4.0 Å. Also, the shortest chlorine-chlorine distance found, 3.699 Å, is between this chlorine and Cl(2)'. Both these distances would become significantly shorter if the Sb-Cl(1) bond were shortened. Thus, it can be inferred that this bond can be readily distorted if more efficient packing of the ions results. The shortening of the Sb-Cl(5) bond appears to be a trans effect in response to the lengthening of the Sb-Cl(1) bond.

The observed bond lengths of the basal antimony-chlorine bonds described above are consistent with characterizing the antimony bonding orbitals as being composed primarily of p-orbitals as in the three-center four-electron bonding scheme described by Porter and Jacobson.³² The lone pair appears to have a comparatively small stereochemical effect. This is supported by the relatively short antimony-antimony distance of 3.932 \AA , where localized lone pairs, if present, would have to be directed toward one another. Distortions of the Cl-Sb-Cl bond angles from the expected 90° (cf. Table VIII) can be explained by interionic repulsions between inversion-related complexes.

The arrangement of the SbCl_5^- complexes in the unit cell is such that the chlorine atoms approximate a closest packed arrangement in the bc plane, as is evident in Figure 5, with the shortest chlorine-chlorine distances approximating the sum of the van der Waal's radii. None of the potassium ions lie between these planes, but rather are located among the SbCl_5^- ions in the planes. The shortest potassium-chlorine distance is 3.147 \AA .

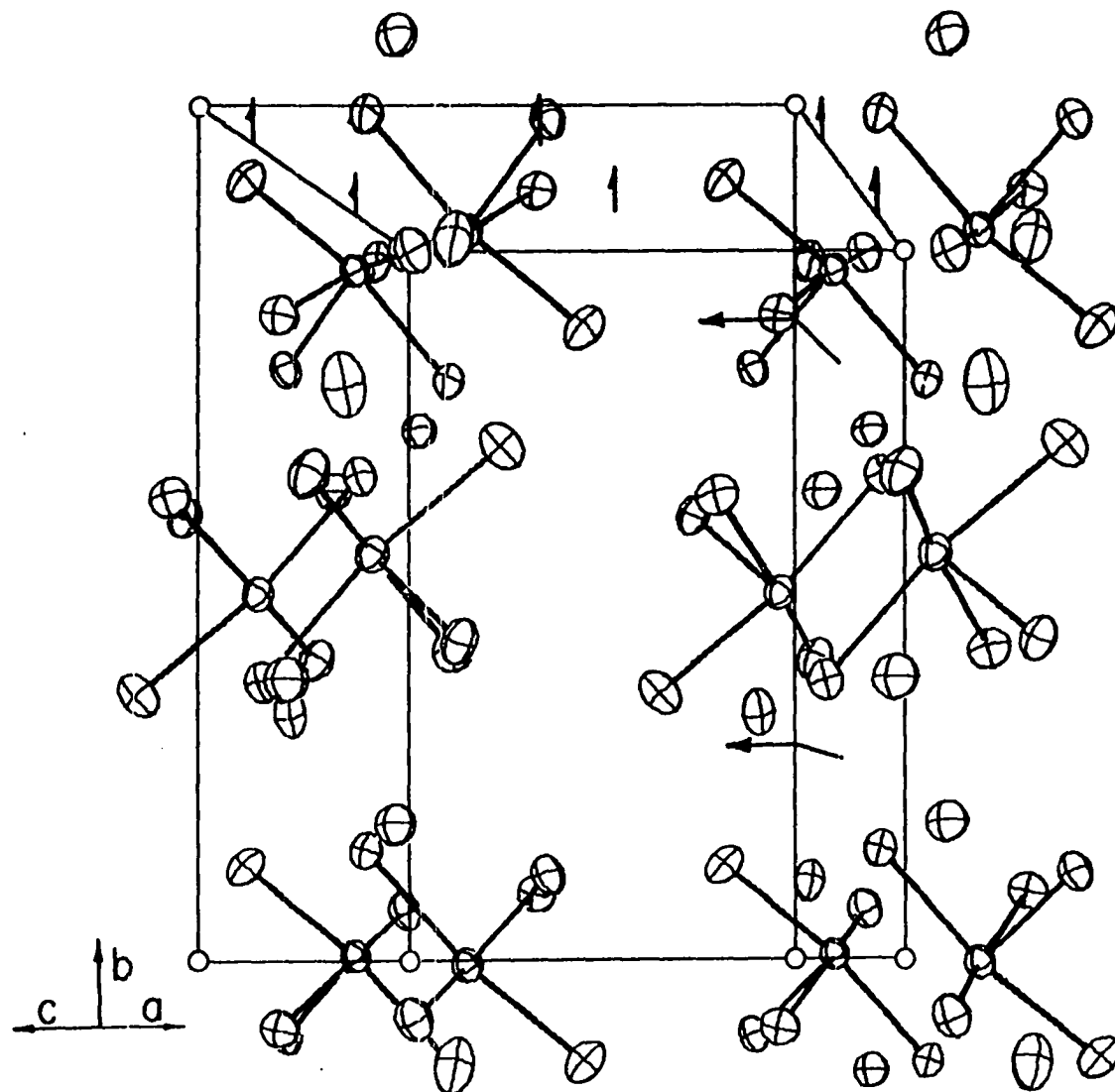


Figure 5. Packing diagram of K_2SbCl_5

ALOP: A PROGRAMMED, SEMI-AUTOMATIC VERSION
OF THE PSEUDO HEAVY ATOM TECHNIQUE

Introduction

The increasing availability of high speed digital computers has enabled the crystallographer to make much more frequent use of mathematical techniques which previously were extremely time consuming. This fact has greatly enhanced the development and usage of direct methods, which recently have evolved to such an extent as to permit semi-automatic solution of crystal structures. In contrast, such indirect methods as Patterson superposition techniques have been employed more and more infrequently in recent times. Despite their great power, these latter methods require a great deal of human intervention and are somewhat tedious to perform. Clearly, what is required is a series of programs which would enable one to solve a structure using superposition techniques but requiring a minimum of human intervention.

This series of programs probably would have greatest applicability to, and thus should be specifically designed to solve, the pseudo heavy atom problem, in which the "heavy" atom does not contribute enough to the phasing to make heavy atom methods feasible. This problem occurs with compounds in which there are many light atoms and but

few heavy atoms, such as transition metal complexes or heavy atom derivatives of organic compounds.

In what follows, the essential features of this series of programs are detailed. The techniques employed naturally divide into two categories: (1) preparation of a Patterson map suitable for evaluation, and (2) utilization of this map to solve the structure.

Map Preparation

A sharpened Patterson map¹¹ is created on either tape or disk by the program ALFF¹⁴ or any other similar Fourier series program. However, in this form the map is somewhat cumbersome to analyze. Hence, the program ALPP (Ames Laboratory Peak Picker) finds and outputs the heights and positions of all the peaks above a certain limit on the Patterson map. ALPP is divided into four subprocedures, the function of which is described below, and a main procedure, which controls the order of execution of the subprocedures. The program listing for ALPP is given in Appendix A.

Input to the first subprocedure, SETUP, consists of the size of the map and the minimum height of a peak which should be recognized. This subprocedure then reads and rewrites the map by layers, setting all points less than the minimum limit equal to zero.

The second subprocedure, LAYERS, reads these map layers and outputs layers with all non-peak grid points negated. The essence of this subprocedure is the subroutine PICKER, which is flowcharted in Figure 6. PICKER analyzes a line of the map point by point. The absolute value of each point is compared with that of the point before it. The lesser of the two is negated. LAYERS calls PICKER for each row and each column of the layer, and then compares points located diagonally to each point, negating those with smaller absolute values.

The next subprocedure, NTRLAY, compares the absolute value of a peak with those of the nine peaks adjacent to it in the next layer, again negating the smaller values. The only positive grid points which now remain are those of peaks. Next, these peak locations and heights are output and the modified map is printed, if desired for debugging purposes.

The final subprocedure, PKSORT, is a modified PL/I translation of QSTSRT. PKSORT sorts the peaks in order of decreasing height and outputs the ordered peaks.

The entire program runs in less core and requires somewhat less execution time than does ALFF. Thus, it is feasible to run the two programs back to back as one job.

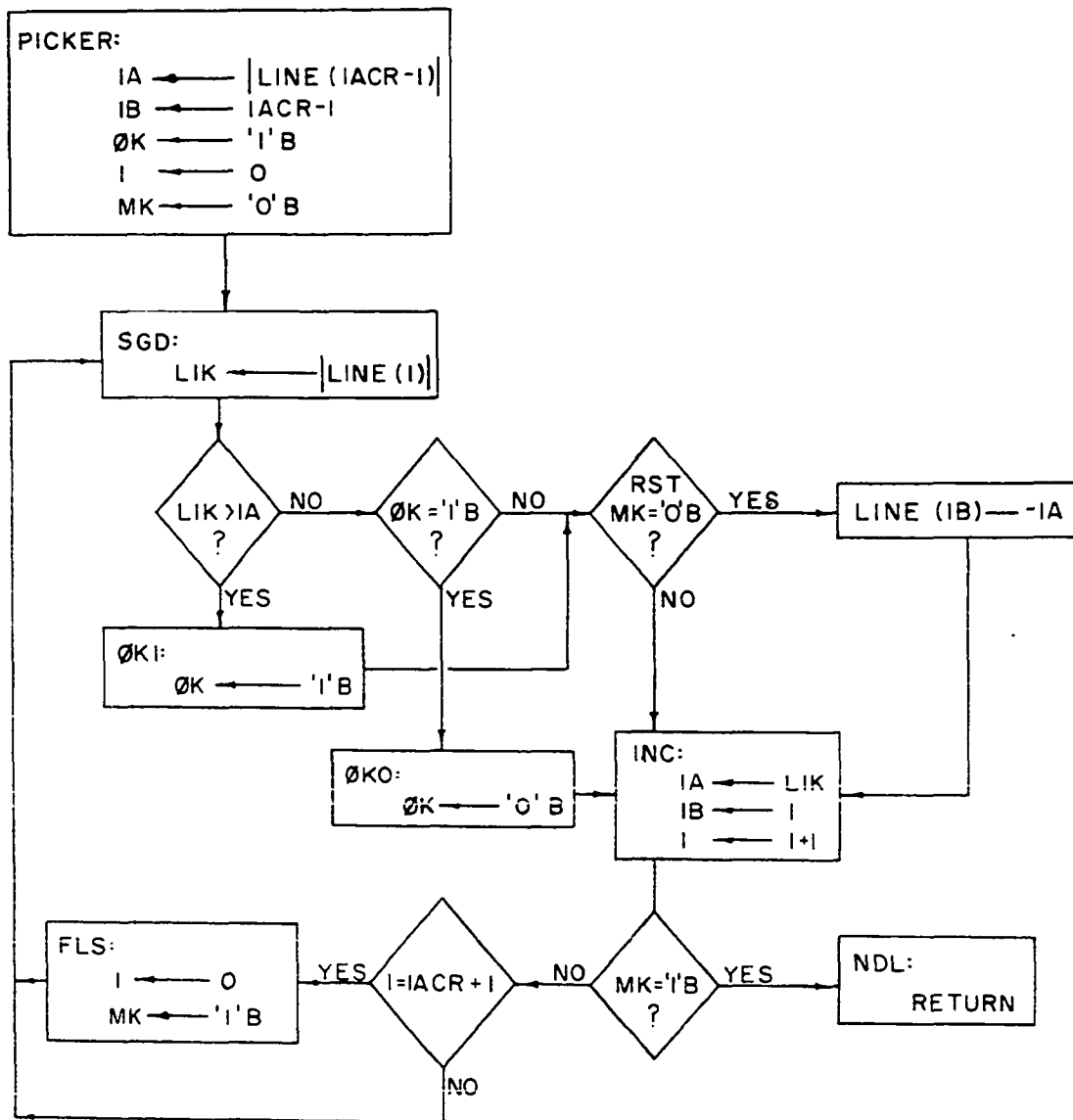


Figure 6. Flowchart of subroutine PICKER

Solution of the Structure

The main program of the series is ALOP (Ames Laboratory Origin Picker), and the program listing is given in Appendix B. ALOP is divided into a main procedure and seven subprocedures.

The main procedure reads in the size of the map, the number of peaks produced by ALPP, and the symmetry operations of the space group under consideration. These are in the form: $p_x x + q_x$, $p_y y + q_y$, $p_z z + q_z$, where p_x , p_y , $p_z = 1$ or -1 and q_x , q_y , $q_z = 0$ or $\frac{1}{2}$. Thus one can represent an equivalent position produced by: an inversion, a two-fold axis, a two-fold screw axis, a mirror plane in one of the three crystal directions or an a-, b-, or c-glide plane. Any of the triclinic, monoclinic, or orthorhombic space groups can be represented by these five symmetry operations (except Fdd2 or Fddd). In addition, any of the other 230 crystallographic space groups can be converted into a space group which only uses these operations, although some loss of symmetry generally occurs.

The first subprocedure, PART1, searches the peaks produced by ALPP for a suitable heavy atom peak. This peak must be among the largest 20% of the peaks. In addition, if any of its coordinates, u , v , w , is equal to 0 or $\frac{1}{2}$ of the unit cell, then it must be at least twice as large as the largest peak which has no one of u , v , w

equal to 0 or $\frac{1}{2}$. These criteria assure that the heavy atom peak chosen is not solely a Harker vector, but allow the choice of a heavy atom which has 0 or $\frac{1}{2}$ as one of its three coordinates, such as the antimony atom in K_2SbCl_5 .

When PART1 finds a suitable heavy atom peak, it prints its coordinates, u_H , v_H , w_H , and uses it as the shift vector of an in-core algebraic superposition. For a peak u , v , w , to be retained, there must also be a peak at $u' = u + u_H$, $v' = v + v_H$, $w' = w + w_H$ in the list of peaks produced by ALPP. In practice, since ALPP only determines the maximum grid point, and not the center, of each peak, these requirements are somewhat too stringent and thus u' , v' , w' is permitted to be off by one grid point in each direction. The values of u' , v' , w' thus found are output for subsequent use.

PART2 assumes that the peaks produced by PART1 represent an electron density map of the compound, with its origin shifted to t_x , t_y , t_z , i.e., the following relations hold: $u_i = x_i + t_x$, $v_i = y_i + t_y$, $w_i = z_i + t_z$, where x_i , y_i , z_i are the coordinates of the peak in electron density space. When the symmetry operations defined above are applied to a peak at x , y , z they produce an equivalent peak at $p_x x + q_x$, $p_y y + q_y$, $p_z z + q_z$. Thus for every peak at $u = x + t_x$, $v = y + t_y$, $w = z + t_z$ there is an equivalent peak at $u' = p_x x + t_x + q_x$, $v' = p_y y + t_y$

+ q_y , $w' = p_z z + t_z + q_z$. In Table X the results of subtracting and adding u , v , w and u' , v' , w' are given for all permutations of p_x , p_y , p_z . The asterisked (*) sums determine values of t_x , t_y , and t_z . PART2 and PART3 accumulate all possible values of t_x , t_y , and t_z for the symmetry operations, as shown in Table XI. PART3 and PART4 write these values, along with the frequency of occurrence of each, on file SORTIN for future use. If any one of t_x , t_y , t_z is not determined, as is the case with all but inversion symmetry, it is set equal to -1. In addition to writing out the exact values of t_x , t_y , and t_z , those which are as much as one grid point off in each direction are also written out. Tables X and XI also demonstrate that values of t_x , t_y , t_z determined by two-folds, screws, mirrors, and glides have to meet criteria before they are acceptable, whereas inversions do not. Therefore, a greater weight is placed on these former values.

At this point, the following items may be present on file SORTIN: t_x , t_y , t_z triples; t_x , t_y ; t_y , t_z ; or t_x , t_z doubles; or t_x , t_y , or t_z singles. These are sorted by the IBM procedure IHESRTA within their different types in order of decreasing frequency of occurrence. PART5 reads and stores 1/64 of the triples, 1/16 of the doubles, and 1/4 of the singles, all of which have the largest frequencies. These singles, doubles, and triples

Table X. Relationships used in determining t_x , t_y , t_z

Quantity	u	v	w
U	$A = x + t_x$	$B = y + t_y$	$C = z + t_z$
U_0	$A + a_x$	$B + a_y$	$C + a_z$
$U_0 + U$	$2A + a_x$	$2B + a_y$	$2C + a_z$
$U_0 - U$	a_x	a_y	a_z
U_1	$-x + t_x + a_x$	$B + a_y$	$C + a_z$
$U_1 + U$	* $2t_x + a_x$	$2B + a_y$	$2C + a_z$
$U_1 - U$	$-2x + a_x$	a_y	a_z
U_2	$A + a_x$	$-y + t_y + a_y$	$C + a_z$
$U_2 + U$	$2A + a_x$	* $2t_y + a_y$	$2C + a_z$
$U_2 - U$	a_x	$-2y + a_y$	a_z
U_3	$-x + t_x + a_x$	$-y + t_y + a_y$	$C + a_z$
$U_3 + U$	* $2t_x + a_x$	* $2t_y + a_y$	$2C + a_z$
$U_3 - U$	$-2x + a_x$	$-2y + a_y$	a_z
U_4	$A + a_x$	$B + a_y$	$-z + t_z + a_z$
$U_4 + U$	$2A + a_x$	$2B + a_y$	* $2t_z + a_z$
$U_4 - U$	a_x	a_y	$-2z + a_z$
U_5	$-x + t_x + a_x$	$B + a_y$	$-z + t_z + a_z$
$U_5 + U$	* $2t_x + a_x$	$2B + a_y$	* $2t_z + a_z$
$U_5 - U$	$-2x + a_x$	a_y	$-2z + a_z$

Table X. (Continued)

Quantity	u	v	w
U_6	$A + q_x$	$-y + t_y + q_y$	$-z + t_z + q_z$
$U_6 + U$	$2A + q_x$	* $2t_y + q_y$	* $2t_z + q_z$
$U_6 - U$	q_x	$2y + q_y$	$2z + q_z$
U_7	$-x + t_x + q_x$	$-y + t_y + q_y$	$-z + t_z + q_z$
$U_7 + U$	* $2t_x + q_x$	* $2t_y + q_y$	* $2t_z + q_z$
$U_7 - U$	$2x + q_x$	$2y + q_y$	$2z + t_z$

Table XI. Restrictions placed on the determination of t_x , t_y , t_z by the type of symmetry element

Type of symmetry element	Determines	Restrictions
Plane perpendicular to x	t_x	$v_1 - v = q_y, w_1 - w = q_z$
Plane perpendicular to y	t_y	$u_2 - u = q_x, w_2 - w = q_z$
Plane perpendicular to z	t_z	$u_4 - u = q_x, v_4 - v = q_y$
Axis in x	t_y, t_z	$u_6 - u = q_x$
Axis in y	t_x, t_z	$v_5 - v = q_y$
Axis in z	t_x, t_y	$w_3 - w = q_z$
Inversion	t_x, t_y, t_z	None

are then merged with each other as described in Table XII, with a latitude of one grid point allowed in each direction. Thus, if a single in t_x equals the t_x of a t_x, t_y double or is off by one grid point, then the frequency of the t_x, t_y double is increased by the frequency of the single. A record is kept of each such merge.

This record is used in PART6, where all of the possible mergings for each symmetry element present are computed. Consider, as an example, the space group $P2_1/c$ which has an inversion producing a triple t_x, t_y, t_z , a two-fold screw axis producing a double in t_x, t_z and a c -glide producing a single in t_y . PART5 should have merged a single in t_y and a double in t_x, t_z with each triple and left a record of having done so. The values of the triples which were not suitably merged are eliminated, and the triple remaining with the highest frequency of occurrence is then output for use in PART7.

Sometimes, however, a space group may not have an inversion. If it has three two-fold or screw axes, these will produce three doubles: $t_{x1} t_{y1}, t_{x2} t_{z2}, t_{y3} t_{z3}$. In the cases where $t_{x1} = t_{x2}, t_{y1} = t_{y3},$ and $t_{z2} = t_{z3},$ a triple is created with a frequency equal to the sum of the frequencies of the three doubles. The highest such triple is then taken as the origin. If any one of $t_x, t_y,$ or t_z is not determined by the above procedures, it

Table XII. Merging of singles and doubles into doubles and triples

Single or double	Double or triple merged into
t_x	$t_x t_y, t_x t_z, t_x t_y t_z$
t_y	$t_x t_y, t_y t_z, t_x t_y t_z$
t_z	$t_x t_z, t_y t_z, t_x t_y t_z$
$t_x t_y$	$t_x t_z, t_y t_z, t_x t_y t_z$
$t_x t_z$	$t_x t_y, t_y t_z, t_x t_y t_z$
$t_y t_z$	$t_x t_y, t_x t_z, t_x t_y t_z$

is set to zero, as the origin may have any value in that direction.

PART7 computes the electron density space coordinates of all the peaks found in PART1 by using the equations: $x_i = u_i - t_x$, $y_i = v_i - t_y$, $z_i = w_i - t_z$. For each peak, this procedure then attempts to find the symmetry equivalent peaks. If at least half of the equivalent peaks are present, a peak is output with the appropriate fractional coordinates.

ALOP uses less than 32K words of main core storage and runs in less than five minutes of CPU time for a 32 x 32 x 32 map with less than 500 peaks input from ALPP.

Results

The programs ALPP and ALOP were tried on two different problems and the technique was successful in both cases. In the first case, the structure of D-(1,5)-glucono lactone (space group $P2_12_12_1$)³³ was "chlorinated" by substituting chlorines for two of the hydrogens, yielding a molecule with two chlorines, six oxygens, and six carbons. The heavy atom ratio for this compound was $\sum Z_{\text{heavy}}^2 / \sum (Z_{\text{light}})^2 = 0.963$. All of the non-hydrogen atoms were used in a structure factor calculation and a sharpened Patterson map was computed from these structure factors. ALPP found 502 off-origin peaks in this map with heights rang-

ing from 13 to 234. A heavy atom peak, which proved to be an oxygen-chlorine vector, was found at $u = 30$, $v = 26$, $w = 3$ with a height of 99 on the $32 \times 32 \times 32$ map. In-core superposition retained 187 peaks with a minimum height of 23. This is a good demonstration of how the superposition process tends to eliminate spurious peaks. Multiple merging produced eleven possible origins, of which the one with the highest frequency of occurrence was $t_x = 14$, $t_y = 13$, $t_z = 12$. When this value was used as an origin, 33 symmetry independent peaks were retained. Subsequent least square refinement of the positional parameters and atom multipliers of these 33 positions through twelve least squares cycles resulted in a conventional discrepancy factor of $R = 0.206$. The scattering factor curve for this and the subsequent test case is defined by:

$$\hat{f}_i = \frac{\sum_{j=1}^N f_{ij}}{\sum_{j=1}^N Z_j},$$

where f_{ij} is the normal scattering factor for the j^{th} atom over a range of $\sin\theta/\lambda$,¹⁵ Z_j is the atomic number of the j^{th} atom, and the sum is over all the atoms in the unit cell.

The second test case was that of K_2SbCl_5 which crystallizes in space group $P2_1/c$ with four eight-atom moieties per unit cell. The heavy atom ratio for this compound is 1.200. ALPP found 258 off-origin peaks on the sharpened

Patterson map, ranging in height from 17 to 508. A heavy atom peak, which was produced by an antimony-antimony vector, was found at $u = 20$, $v = 16$, $w = 3$ with a height of 282 on the $32 \times 32 \times 32$ map. In-core superposition retained 112 peaks. The origin with the highest frequency of occurrence was at $t_x = 10$, $t_y = 0$, $t_z = 9$, and its use yielded 20 symmetry independent peaks. Sixteen cycles of full matrix least squares refinement of the positional parameters and atom multipliers of these positions led to the removal of eleven of them as their atom multipliers dropped to less than 0.40. The remaining nine positions refined to yield a conventional discrepancy factor of $R = 0.240$.

PSST: A COMBINATION OF PATTERSON SUPERPOSITION
AND SIGMA-2 TECHNIQUES FOR PHASE DETERMINATION

Introduction

At present there are two methods commonly used for solving structures of moderate complexity. Direct methods, such as those using the Σ_2 relation,³⁴ are primarily reciprocal space methods, while methods based on the deconvolution of the Patterson function (for a detailed bibliography see Buerger³⁵) are primarily real space methods.

There is a certain parallelism between these two methods and both have their advantages and disadvantages. Both involve some initial choices which can greatly influence the success of the method. The Σ_2 relation can be readily programmed and many automatic or semi-automatic procedures have been developed based on this relation. However, it is usually difficult to make use of known structural information in this approach. Furthermore, if no reasonable structure is produced, the investigator has little recourse but to modify his choice of origin-determining reflections or to closely examine those phases selected at the early and most critical part of this phase determination procedure. With Patterson methods, on the other hand, there are usually a greater number of options initially available corresponding to differing modes of

selection of peaks for superposition. Also, known structural information can be more readily introduced, since a real space representation is being employed. For complex structures, however, large numbers of superpositions are generally required and severe degradation of the structural image can result due to the accumulation of errors in the atom position selections.

The advent of the fast Fourier transform technique and its application to crystallography³⁶ allows rapid real space - reciprocal space conversions. Thus, it is appropriate to consider whether a hybrid direct method - Patterson method approach having greater power than either method alone can be developed. It is just such a hybrid that is described here.

Theoretical Basis of the Method

In direct methods employing the Σ_2 relation, one starts with E's of large magnitude so that phases will be determined with reasonably high probabilities. Due to the fact that the initial contributors are few in number, erroneous phase indications may still result which then propagate in the phase determination procedure. Consider the map produced by a Fourier transform using as non-zero coefficients only those reflections input into the Σ_2 relation (henceforth this map will be referred to as the Σ_2 map). For the phase determination procedure to be successful, it

is necessary that the square of this Σ_2 -map better resemble the true electron density function than does the Σ_2 -map itself. If so, the phases of the transformed coefficients with larger magnitudes should be good approximations to the phases of the corresponding large $|E|$'s.

Since the initial set of E's is very small in number, possibly only the three origin-determining reflections, it is the characteristics of the Σ_2 -map which should be closely examined. First, if large $|E|$'s are used, there is a high probability that atoms will lie on, or at least near, some of the maxima occurring on this map. Second, there will be a large number of extraneous maxima on the square of the Σ_2 -map -- a number far exceeding the number of atoms in the cell. The first is an asset and the second a liability for successful phase determination. These extraneous peaks come from either maxima or minima on the Σ_2 -map. It is the presence of these extra peaks that greatly inhibits the production of additional phase information.

One would like to modify the square of the Σ_2 -map so that it better resembles the electron density function. An obvious such modification is to eliminate all negative regions (or possibly regions less than a certain lower bound) by setting these regions equal to zero before squaring. Indeed, this technique has been applied by Barrett

and Zwick³⁷ to some extent in the extension and refinement of crystallographic protein phases.

In the initial application of the Σ_2 relation, there are so few phased E's that even with the modification described above, there are large positive regions in many areas of the map which do not correspond to atomic locations. However, the Patterson function contains images of the structure with each atom in turn at the origin. Therefore, if an atomic position can be selected on the Σ_2 -map, a superposition of the appropriately scaled Patterson map on this position should produce a map with considerably fewer extraneous peaks and with much better resemblance to the electron density function. If such a map is then squared to emphasize the higher peaks and transformed, better and more extensive phase information will result. Once a sufficiently large set of phased E's has been obtained, the remaining $|E|$'s can be efficiently phased by normal application of phase extension and refinement techniques of the Σ_2 type.

Application of the Method

Centric case

The compound β -picoline-N-oxide fumaric acid adduct³⁸ was chosen as a centrosymmetric test case. We felt this would be a good test case as the structure had previously been solved only with difficulty by use of a roving model --

vector verification technique after usual superposition and symbolic addition procedures had not proved successful.

This adduct crystallizes in the space group $P2_1/c$ with $a = 3.888$, $b = 14.194$, $c = 14.666$ Å and $\beta = 98.85^\circ$. There are two adducts of formula $C_{16}H_{18}N_2O_{12}$ per unit cell, i.e., the adduct has a center of symmetry. Values of $|E|$ were computed in the ordinary way and there were 270 $|E|$'s greater than 1.0. The three selected origin-determining reflections are given in Table XIII. These three, along with the symmetry-related reflections, were used in a Σ_2 -map calculation (32 x 32 x 32 grid points). Some typical sections of this map are shown in Figure 7.

The positions of the five highest peaks on this map were noted and in each case checked by examining the Patterson for the presence of vectors between symmetry-related atoms. In each case, such vectors were found and indeed these peaks fell approximately (within 0.5 Å) at the positions of four carbons and a nitrogen in the structure.

All of the negative regions in the Σ_2 -map were then set equal to zero and five independent superpositions were carried out by placing the origin of the Patterson at each of the five peak positions and the symmetry-related points. A sharpened Patterson function was used and the minimum procedure employed.³⁹ The scale of the Patterson was

Table XIII. Origin-determining reflections for the centric test case (β -picoline-N-oxide fumaric acid adduct)

h	k	l	E	Sign
1	0	2	4.17	+
3	1	3	2.53	-
1	14	-5	2.14	+

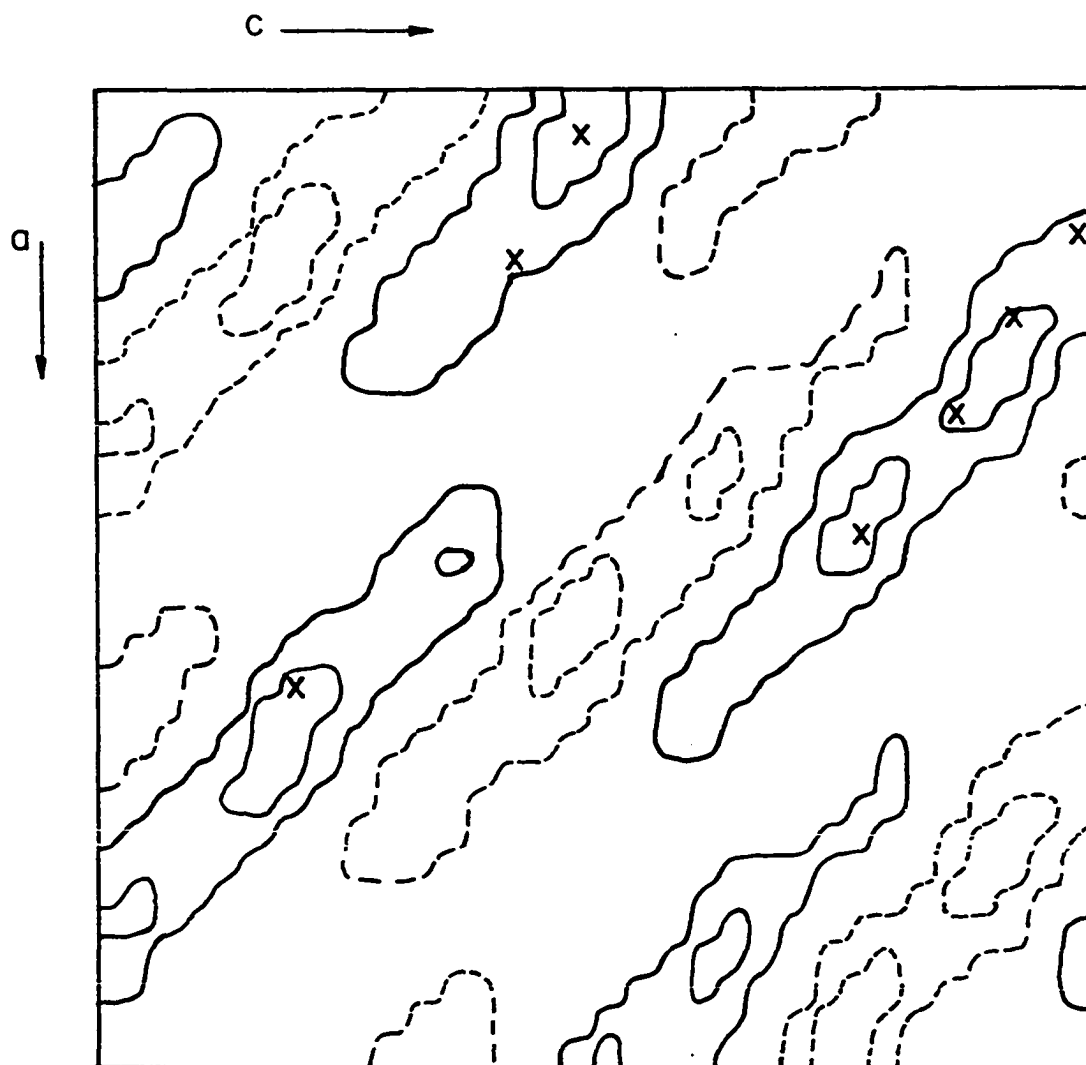


Figure 7a. Composite of layers 3,4,5 of a Σ_2 -map for β -picoline-N-oxide fumaric acid adduct.
— contoured at 40 and 80. ---- contoured at -40 and -80. Atom positions indicated by X.

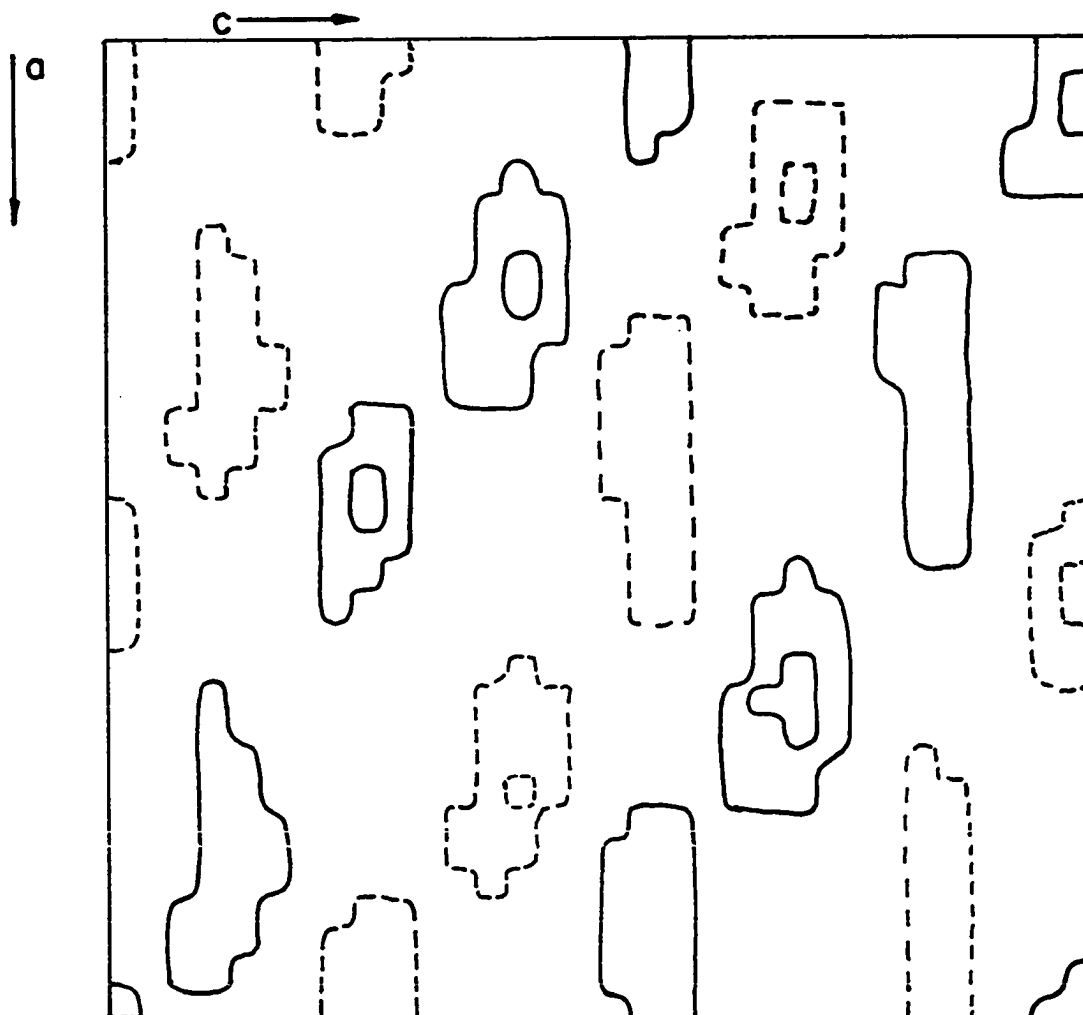


Figure 7b. Layer 9 of a Σ_2 -map for β -picoline-N-oxide fumaric acid adduct. — contoured at 15 and 25. ---- contoured at -15 and -25. No atoms in or near this section.

adjusted so that the value of the highest off-origin peak on the Patterson map was approximately equal to the value of the highest off-origin peak on the Σ_2 -map. Figure 8 shows some typical results using the peak corresponding to the nitrogen atom position as the superposition point.

Each of the five maps was then squared and the resulting transform coefficients (G_{hkl}) calculated using a fast Fourier algorithm.¹⁴ Only the 50 reflections with the largest values of the product $|E*G|$ and with $|E| > 1.50$ were kept. Some typical results are shown in Table XIV. The signs determined for each hkl were then averaged. (In some cases more than 80% of the 50 largest $|E|$'s were signed correctly in the individual sets.) These signed reflections were then used to compute a new Σ_2 -type map, and negative regions were set equal to zero. The transform of the square of this map was used to obtain signs (92% of which were correct) for input at the 90% confidence level into a phase extending program.⁴⁰ The resulting complete set of 270 phases was used to compute a map from which the positions of all the non-hydrogen atoms in the structure were readily determined. There were no significant spurious peaks on this map. This method has recently been used to solve the structure of diisopropyl-(2,3,4,5-tetraphenyl-cyclopenta-2,4-diene)-phosphate, which crystallizes in space group $P2_1/c$ with 160 non-

Table XIV. Representative results^a obtained for a centric test case (β -picoline-N-oxide fumaric acid adduct)

h	k	l	E	Calculated signs					Known sign
				1	2	3	4	5	
-2	10	4	3.25	-	+	+	+	+	+
-1	11	7	3.13	-	+	+		+	+
0	11	9	3.00	-		+			+
0	12	4	2.94				+		-
-1	10	12	2.80	-	-	-	-	-	-
1	10	8	2.73	+	-	-		-	-
-2	4	12	2.63				+		+
1	11	7	2.55	+	-			-	-

^a The absence of a calculated sign indicates that the value of $|E*G|$ for that reflection was smaller than the limit used.

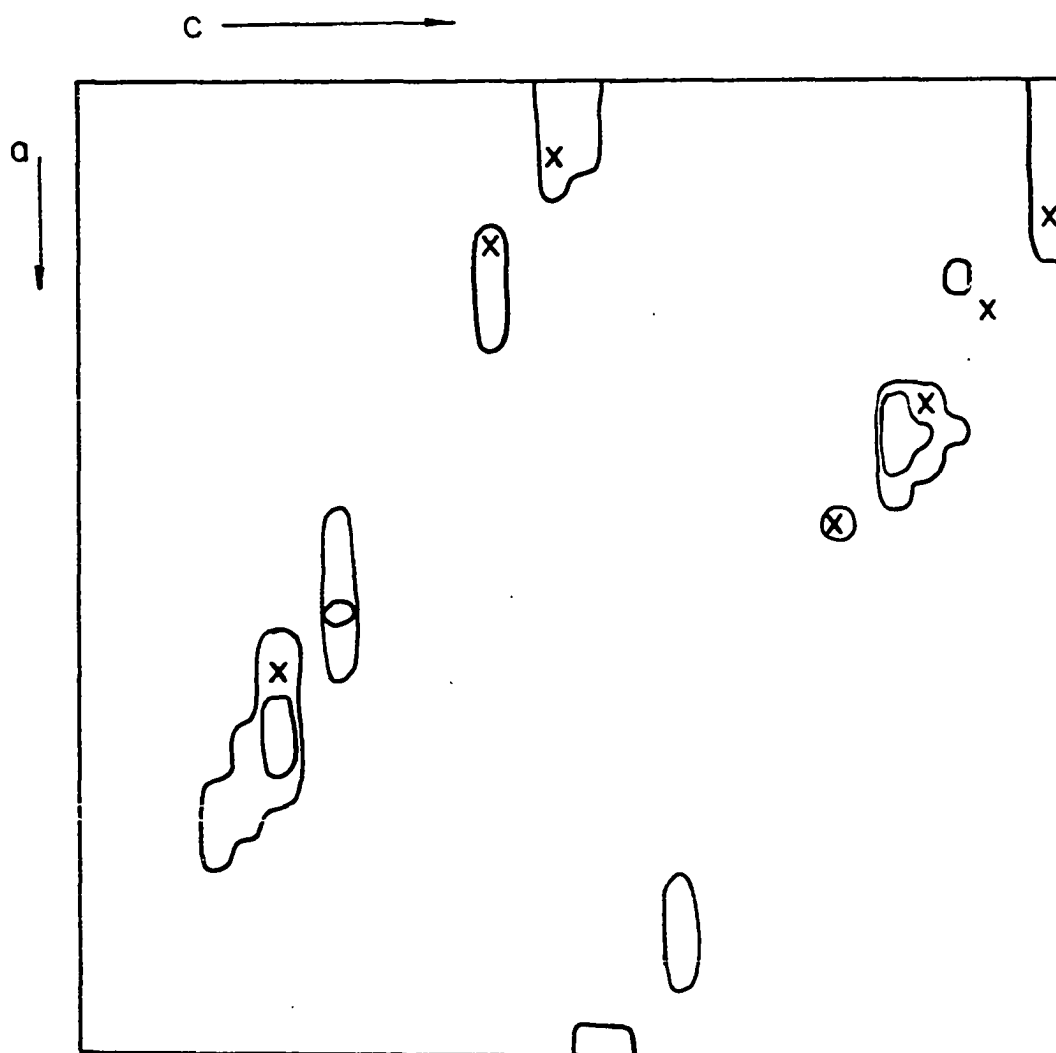


Figure 8a. Results of Patterson map superimposed on the Σ_2 -map of Figure 7 at the four nitrogen equivalent positions. Composite of layers 3,4,5. — contoured at 9 and 18. Atom positions indicated by X.

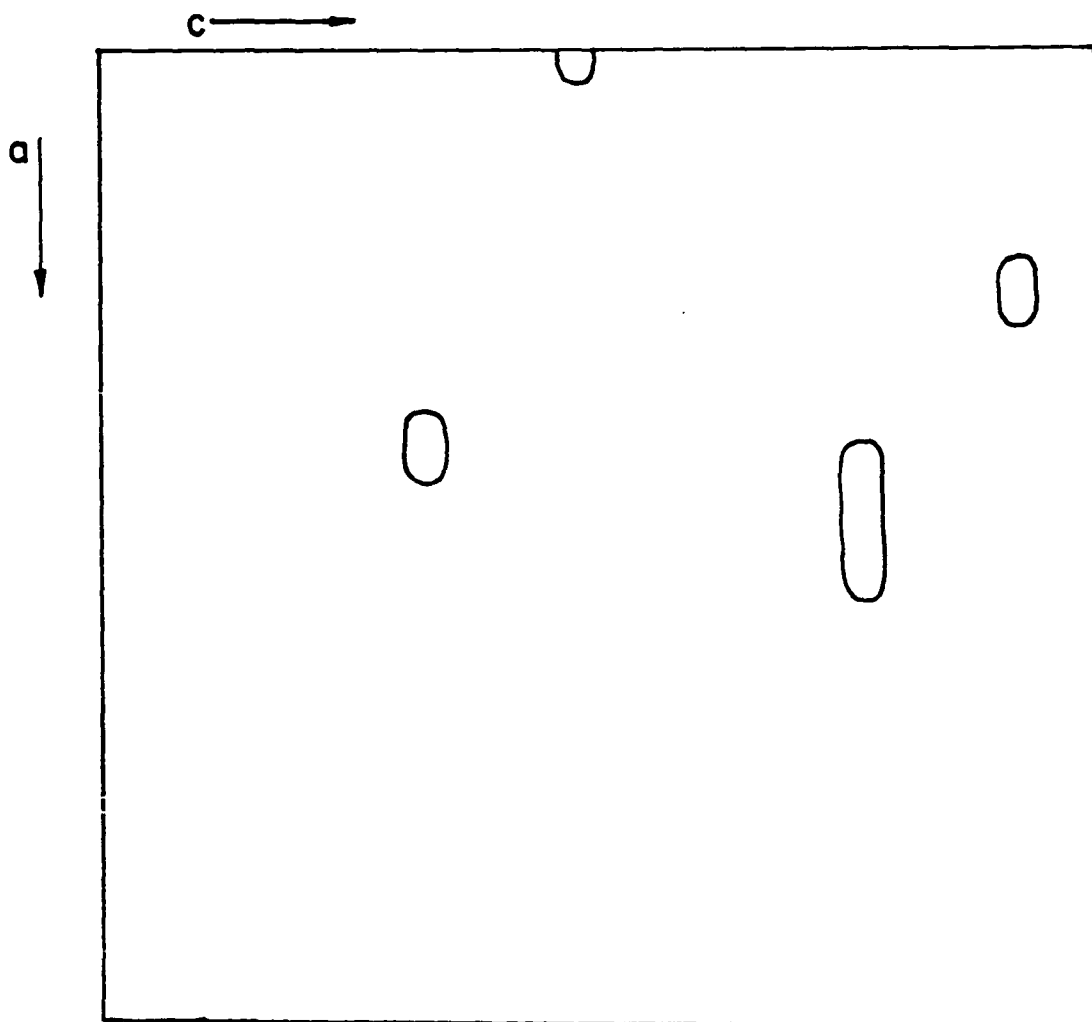


Figure 8b. Results of Patterson map superimposed on the Σ_2 -map of Figure 7 at the four nitrogen equivalent positions. Layer 9. — contoured at 5. No atoms in or near this section.

hydrogen atoms per cell.⁴¹

Acentric case

The compound chosen as a test for the acentric case was D-(1,5)-glucono lactone,³³ which crystallizes in the space group $P2_12_12_1$ with axial lengths $a = 7.838$, $b = 12.322$, $c = 7.544$ Å. Of the 1259 unique observed reflections, 435 have $|E|$ greater than 1.0. Three origin-determining reflections were selected ($|E| = 2.39, 2.51, 2.04$), two of which were non-zonal reflections. To make the test a reasonably severe one, no enantiomorph-selecting reflection was included; the enantiomorph was chosen as part of the superposition procedure.

The Σ_2 -map produced from these and their symmetry-related reflections showed more than 25 large peaks, all of which had relative heights between 120 and 185. The relative height of the other peaks on this map was less than 90. However, only eight of these 25 peaks generated appropriate Harker vectors on the Patterson. Of these eight, four were clearly in one enantiomorph, since they remained when the superposition point was a member of the set.

Using these four peaks and proceeding in a manner similar to the centric case above, the average phases of the 30 largest $|E^*G|$'s with $|E| > 1.40$ were obtained. Some typical results for this acentric structure are given in

Table XV. The transform of the square of the expanded Σ_2 -map yielded initial phases for the 50 largest $|E^*G|$'s with $|E| > 1.40$. These phased E's were then input into a phase-extending program at the 90% confidence level. In the resulting set of 410 phased E's, 390 were within 40° of the published phases and their transform readily revealed all the non-hydrogen atomic positions. As in the centric case, there were no significant spurious peaks on this final map.

Extensions of the Method

Since a reasonably severe test of the method was desired, only three origin-determining reflections were used for the initial Σ_2 -map calculation in each case. Other reflections, phased by either Σ_2 or Σ_1 relations (and perhaps with appropriate weights), can also be included to produce peaks of greater reliability. In the centric case, those Σ_1 reflections which were determined with greater than 90% probability were included in the calculation of the Σ_2 -map. Their addition improved the phase agreement to a small extent. The frequency check procedure⁴² can also be applied to the Σ_2 -map.

It is also possible to include an additional strong reflection in the origin-determining reflections, thus producing two Σ_2 -maps in the centric case, for example. The resulting two sets of averaged phases could then be

Table XV. Representative results^a obtained for an acentric test case (D-(1,5)-glucono lactone)

h	k	l	E	Calculated phases (°)				Known phase
				1	2	3	4	
0	3	6	3.48	270	270	270	270	270
0	4	3	2.67	0	180	180	180	180
0	7	9	2.58		90	90	90	90
0	11	2	2.36	89				90
2	2	6	2.22		277		256	296
1	7	5	2.19			276	284	293
4	-9	-1	2.04	230	243	220	256	252
0	4	0	1.95	179				0
3	-3	-7	1.77	179	171	182	177	197
3	4	2	1.64		261		278	316
1	-3	-2	1.59		83		90	81
0	2	3	1.58	179	0		0	180
2	4	6	1.56	84	88		91	114

^a The absence of a calculated phase indicates that the value of $|E^*G|$ for that reflection was smaller than the limit used.

handled in a similar way as in those direct methods programs which produce multiple solutions.

Lower bounds different from zero can be used for modification of the resultant superposition map. Indeed, some calculations for the centric example have shown that use of a lower bound of 10% of the maximum peak height results in somewhat improved agreement.

From Tables XIV and XV, it is obvious that a straight average is a poor procedure compared to a more judicious method of averaging. Preliminary computations indicate that in the centric case a requirement of a net of two like signs produces a significant improvement in the percentage of correct signs selected.

The phases are also somewhat sensitive to grid point resolution of the maps. In the centric structure, calculations were run using a grid of $0.12 \times 0.45 \times 0.45$ Å resolution. Results improve if a resolution of approximately 0.25 Å is used in all three directions.

Squaring the resultant superposition map appears to give the best phases compared with other powers which could be employed. All exponents from 0.2 to 6.6 in steps of 0.2 were examined for a typical run, with 2.0 appearing the most satisfactory.

RESEARCH PROPOSALS

The proposals for research given below suggested themselves during the course of the research described in this thesis. No claim of an exhaustive literature search for these ideas is implied, although it is the author's belief that they are not presently under investigation.

Due to the fact that more investigators without formal training are employing crystallography as a research tool, there is a desperate need for the development of computer programs which can make many of the routine decisions now requiring human intervention. ALPP eliminates, or at least makes much less tedious, the contouring of a map, and is an example of this type of program. Such a program should be developed to implement the PSST method. One could write a program to implement the heavy atom technique, which would work in conjunction with ALOP, by cycling structure factor and Fourier series calculations, at the same time deciding whether or not possible atomic positions should be retained. As well as being easy for the initiate to use, the above programs should also permit enough intervention so that the course of their execution can be altered by the more experienced user.

The prime difficulties in implementing direct methods are in choosing between various sets of phases

produced and in discriminating spurious from real atomic peaks. The first problem is being extensively researched and such methods as the comparison of absolute figures of merit and the psi zero test of MULTAN,⁴⁰ the absolute value of rho test reported by W. Ozbirn,⁴³ and a plot of psi zero vs. the absolute figure of merit as described by Cochran and Douglas⁴⁴ are all examples of possible solutions. A promising approach to the problem of peak discrimination should be the superposition of the Patterson on a likely atomic position, similar to the technique used in the PSST method. Another approach would be the development of a program which makes use of known interatomic vectors, such as those within a benzene ring, to choose peaks of chemical sense. A third would be the development of a more exact and easily used technique for producing three-dimensional models. A model constructed of wooden spheres suspended by fine lines from a perforated plate would satisfy these requirements.

The relative ease in determining the bonding mode of cyanide in trans-(CN)₂ trien cobalt (III) perchlorate indicates that X-ray diffraction data may be sensitive enough to distinguish between carbon and nitrogen. A more intensive effort on the part of investigators on this problem and perhaps even a reexamination of published data could be initiated.

The number of antimony (III) structures which have been determined is exceedingly small. The investigation of a number of different compounds of formula $M_2Sb^{III}X_5$ ($M = Na, K, Rb, Cs; X = Cl, Br, I$) would be of interest in determining the influence of the M^+ and the X^- on the configuration of the SbX_5^- complex.

The Σ_2 -map has a much wider applicability than is described in the PSSST method. In combination with the discriminator function⁴⁵ to test possible atomic positions, it should have great power. In addition, using the expanded starting set of phased E's to produce a map which then would be used in place of the Σ_2 -map, is an extension which has promise.

APPENDIX A

PROGRAM LISTING OF ALPP

*

-


```

SORT PEAKS INTO DESCENDING ORDER BY HEIGHT AND OUTPUT          */ ALPP0460
                                                                */ ALPP0470
CALL PKSORT(#PEAK);                                           ALPP0480
PUT EDIT ('NORMAL PROGRAM TERMINATION')(PAGE,A);              ALPP0490
END CONTOUR;                                                  ALPP0500

* PROCESS('ATR,XREF,NOSTMT,OPT=02');
/* READ IN THE CONTROL CARDS AND INITIALIZE THE MAP          */ STUP0010
SETUP: PROCEDURE (IACR,IDWN,ILAY,IPRT,LMT,FW,SP,IACS,PMIN,PMAX); */ STUP0020
DECLARE (IACR, IDWN, ILAY, IPRT, LMT, FW, SP, IACS, PMIN,      STUP0030
        PMAX, ISTEP) FIXED BINARY (15);                      STUP0040
DECLARE LNALFF (0:IACR-1) CONTROLLED FLOAT BINARY,           STUP0050
        (LNFOUR(0:IACR), LAYER 10:IACR,0:IDWN))              STUP0060
        CONTROLLED FIXED BINARY (15);                        STUP0070
                                                                STUP0080
DECLARE PGM CHARACTER (4);                                    STUP0090
DECLARE XLM FLOAT BINARY;                                     STUP0100
DECLARE TITLE CHARACTER (80);                                STUP0110
DECLARE MPOUT FILE ENVIRONMENT (REGIONAL(1)) KEYED;          STUP0120
DECLARE STAMP CHARACTER (54) EXTERNAL;                       STUP0130
CALL TM_DT;                                                  STUP0140
                                                                STUP0150
/* READ AND INTERPRET THE CONTROL CARDS                        */ STUP0160
                                                                */ STUP0170
GET EDIT (TITLE,PGM,IACR,IDWN,ILAY,IPRT,LMT,FW,SP,IMUD)      STUP0180
        (A(80),A(4),7 F(4),X(44),F(4));                      STUP0190
CLOSE FILE (SYSIN);                                          STUP0200
PUT EDIT (TITLE, STAMP,                                       STUP0210
        'NUMBER OF GRIDS ACROSS A FULL LINE =',IACR,        STUP0220
        'NUMBER OF LINES DOWN A FULL LAYER = ',IDWN,       STUP0230
        'NUMBER OF LAYERS IN A FULL MAP =',ILAY,           STUP0240
        'LOWER LIMIT OF A RECOGNIZABLE PEAK = ',LMT)       STUP0250
        (A(80),SKIP(2),X(20),A(54),4 (SKIP(2),X(25),A,    STUP0260
        COL(65),F(4)));                                       STUP0270
PUT EDIT ('THE GENERATING PROGRAM WAS "',PGM,'"')          STUP0280
        (SKIP(2),X(20),A,A(4),A);                            STUP0290
                                                                STUP0300
IACS = 0;                                                    STUP0310
IF (IPRT=1) THEN PRTR: DO;                                    STUP0320
        PUT EDIT ('THE MAP WILL BE PRINTED')(SKIP(2),X(25),A);
PUT EDIT ('FIELD WIDTH =',FW,'SPACES BETWEEN LINES =',SP)  STUP0330
        (2 (SKIP(2),X(25),A,F(4)));                          STUP0340
CALL PRSETUP (IACS,IACR,FW,SP,PMIN,PMAX,ISTP);             STUP0350
IF (ISTP=1) THEN GO TO ABND; ELSE;                          STUP0360
        END PRTR; ELSE PUT EDIT ('THE MAP WILL NOT BE PRINTED')
        (SKIP(2),X(25),A); ELSE;                            STUP0370
                                                                STUP0380
IF (PGM='ALFF') THEN ALLOCATE LNALFF; ELSE;                 STUP0390
ALLOCATE LNFOUR, LAYER;                                     STUP0400
PUT PAGE;                                                  STUP0410

```



```

OPEN FILE (MAPIN) INPUT RECORD SEQUENTIAL,
FILE (MPOUT) OUTPUT RECORD SEQUENTIAL;
/*
READ MAP LINES, ZERO POINTS LESS THAN LMT, & WRITE MAP LAYERS
*/
IF (PGM='ALFF') THEN DO; XLM = LMT;
NLAY = ILAY-1; NDWN = IDWN-1; END;
ELSE DO; NLAY = ILAY - 1; NDWN = IDWN; END;
LYLUP: DO L = 0 TO NLAY BY 1;
LNLUP: DO K = 0 TO NDWN BY 1;
IF (PGM='ALFF') THEN AL: DO;
GDLUP: READ FILE (MAPIN) INTO (LNALFF);
DO J = 0 TO IACR-1 BY 1;
IF (LNALFF(J)<=XLM) THEN LAYER (J,K) = 0;
ELSE LAYER (J,K) = LNALFF(J);
END GDLUP;
LAYER(IACR,K) = LAYER(0,K);
END AL;
PTLUP: READ FILE (MAPIN) INTO (LNFOUR);
DO J = 0 TO IACR BY 1;
IF (LNFOUR(J)<=LMT) THEN LAYER (J,K) = 0;
ELSE LAYER (J,K) = LNFOUR (J);
END PTLUP;
END FR;
END LNLUP;
LAYER(*,IACR) = LAYER(*,0);
WRITE FILE (MPOUT) FROM (LAYER) KEYFROM(L);
PUT EDIT ('LAYER NUMBER ',L,' WRITTEN OUT.')
(SKIP,A,F(3),A);
END LYLUP;
FREE LNALFF, LNFOUR, LAYER;
CLOSE FILE (MAPIN), FILE (MPOUT);
RETURN;
ABND: END SETUP;

```

```

STUP0420
STUP0430
STUP0440
STUP0450
STUP0460
STUP0470
STUP0480
STUP0490
STUP0500
STUP0510
STUP0520
STUP0530
STUP0540
STUP0550
STUP0560
STUP0570
STUP0580
STUP0590
STUP0600
STUP0610
STUP0620
STUP0630
STUP0640
STUP0650
STUP0660
STUP0670
STUP0680
STUP0690
STUP0700
STUP0710
STUP0720
STUP0730
STUP0740
STUP0750
STUP0760
STUP0770

```

```

* PROCESS('ATR,XREF,NOSTMT,OPT=02');
/* CREATES A TIME - DATE STAMP FOR FUTURE USE
(SUBRG,STRG): TM,DT: PROCEDURE;
DECLARE STAMP CHARACTER(54) EXTERNAL, AMPM CHARACTER(4);
DECLARE MOS(12) CHARACTER(9) VARYING INITIAL ('JANUARY','FEBRUARY',
'MARCH','APRIL','MAY','JUNE','JULY','AUGUST','SEPTEMBER',
'OCTOBER','NOVEMBER','DECEMBER');
DECLARE TM CHARACTER(9), TMS(2) CHARACTER(2) DEFINED TM; TM = TIME;
DECLARE DT CHARACTER(6), DS (3) CHARACTER(2) DEFINED DT; DT = DATE;
IF (TMS(1) > 11) THEN AMPM = 'P.M.'; ELSE AMPM = 'A.M.';

```

```

TMDT0010
TMDT0020
TMDT0030
TMDT0040
TMDT0050
TMDT0060
TMDT0070
TMDT0080
TMDT0090
TMDT0100

```



```

RTN:      J = J + FW;
          SUBSTR(HEAD,J,FW) = NUMS(I);
          ISTOP = 0;
          RETURN;
TERM:     ISTOP = 1;
          GO TO RTN;
          END PRSETUP;
END HD;
PRSU0440
PRSU0450
PRSU0460
PRSU0470
PRSU0480
PRSU0490
PRSU0500

```

```

/* PICK PEAKS FROM EACH LAYER AND WRITE OUT THE REVISED LAYERS */
LAYERS:  PROCEDURE (IACR, IDWN, ILAY, FW, SP, IACS, PMIN, PMAX);
          DECLARE (IACR, IDWN, ILAY, FW, SP, IACS, PMIN, PMAX)
          FIXED BINARY (15);
          DECLARE MPOUT FILE ENVIRONMENT (REGIONAL(1)) KEYED;
          DECLARE (LNACR(0:IACR), LNDWN(0:IDWN), LAYER(0:IACR,0:IDWN))
          CONTROLLED FIXED BINARY;
          OPEN FILE (MPOUT) UPDATE RECORD DIRECT;
          ALLOCATE LAYER, LNDWN, LNACR;
          PUT PAGE;
/*
          FIND THE PEAKS LAYER BY LAYER
LAYLP:   DO L = 0 TO ILAY-1 BY 1;
          READ FILE (MPOUT) INTO (LAYER) KEY (L);
/*
          GO THROUGH THE LAYERS ROW BY ROW
LINLP:   DO K = 0 TO IDWN BY 1;
          LNACR(*) = LAYER (*,K);
          CALL PICKER (LNACR, IACR);
          LAYER(*,K) = LNACR;
          END LINLP;
/*
          GO THROUGH THE LAYERS COLUMN BY COLUMN
COLUP:   DO J = 0 TO IACR BY 1;
          LNDWN = LAYER (J,*);
          CALL PICKER (LNDWN, IDWN);
          LAYER(J,*) = LNDWN;
          END COLUP;
/*
          CHECK DIAGONAL ELEMENTS
KLUP:    DO K = 0 TO IDWN BY 1;
          IF (K=0) THEN IDM = IDWN - 1;
          ELSE IDM = K - 1;
          IF (K=IDWN) THEN IOP = 1;

```

```

LYRS0010
LYRS0020
LYRS0030
LYRS0040
LYRS0050
LYRS0060
LYRS0070
LYRS0080
LYRS0090
LYRS0100
LYRS0110
LYRS0120
LYRS0130
LYRS0140
LYRS0150
LYRS0160
LYRS0170
LYRS0180
LYRS0190
LYRS0200
LYRS0210
LYRS0220
LYRS0230
LYRS0240
LYRS0250
LYRS0260
LYRS0270
LYRS0280
LYRS0290
LYRS0300
LYRS0310
LYRS0320
LYRS0330
LYRS0340
LYRS0350
LYRS0360
LYRS0370
LYRS0380
LYRS0390

```

```

JLUP: DO J = 0 TO IACR BY 1;
      IF (LAYER(J,K) = 0) THEN GO TO NDJL;
      IF (J=0) THEN IAM = IACR - 1;
      ELSE IAM = J - 1;
      IF (J=IACR) THEN IAP = 1;
      ELSE IAP = J + 1;
      LJK = LAYER(J,K);
      LAJK = ABS(LAYER(J,K));
      IF (ABS(LAYER(IAP,IDP)) > LAJK) THEN LJK = -LAJK;
      ELSE LAYER(IAP,IDP) = -ABS(LAYER(IAP,IDP));
      IF (ABS(LAYER(IAP,IDM)) > LAJK) THEN LJK = -LAJK;
      ELSE LAYER(IAP,IDM) = -ABS(LAYER(IAP,IDM));
      IF (ABS(LAYER(IAM,IDP)) > LAJK) THEN LJK = -LAJK;
      ELSE LAYER(IAM,IDP) = -ABS(LAYER(IAM,IDP));
      IF (ABS(LAYER(IAM,IDM)) > LAJK) THEN LJK = -LAJK;
      ELSE LAYER(IAM,IDM) = -ABS(LAYER(IAM,IDM));
      LAYER(J,K) = LJK;
NDJL: END JLUP;
      END KLUP;
/*
      OUTPUT THE CONTOURED MAP LAYER
      REWRITE FILE (MPOUT) FROM (LAYER) KEY (L);
      PUT EDIT ('PEAK-PICKED LAYER ',L,' HAS BEEN REWRITTEN.')
      (SKIP,A,F(3),A);
      END LAYLP;
      RETURN;
      END LAYERS;

```

```

LYRS0400
LYRS0410
ELSE; LYRS0420
LYRS0430
LYRS0440
LYRS0450
LYRS0460
LYRS0470
LYRS0480
LYRS0490
LYRS0500
LYRS0510
LYRS0520
LYRS0530
LYRS0540
LYRS0550
LYRS0560
LYRS0570
LYRS0580
LYRS0590
LYRS0600
LYRS0610
*/ LYRS0620
LYRS0630
LYRS0640
LYRS0650
LYRS0660
LYRS0670
LYRS0680

```

```

* PROCESS('ATR,XREF,NOSTMT,OPT=02');
/* PROCEDURE TO CONTOUR A LINE
PICKER: PROCEDURE (LINE,IACR);
        DECLARE LINE (*);
        DECLARE (IACR,IA,IB,I,LIK) FIXED BINARY (15);
        DECLARE (OK,MK) FIXED BINARY (15);
        BIT (1);
        IA = ABS (LINE(IACR-1));
        IB = IACR - 1;
        OK = '1'B;
        I = 0;
        MK = '0'B;
SGD: LIK = ABS (LINE(I));
      IF (LIK > IA) THEN GO TO OK1;
      IF (OK) THEN GO TO OK0;
      ELSE GO TO RST; ELSE
OK0: OK = '0'B;
      GO TO INC;
OK1: OK = '1'B;

```

```

*/ PIKR0010
PIKR0020
PIKR0030
PIKR0040
PIKR0050
PIKR0060
PIKR0070
PIKR0080
PIKR0090
PIKR0100
PIKR0110
PIKR0120
PIKR0130
PIKR0140
PIKR0150
PIKR0160
PIKR0170

```

```

RST:      IF (-MK) THEN LINE(IB) = -IA;                               ELSE;    PIKR0180
INC:      IA = LIK;                                                  PIKR0190
          IB = I;                                                    PIKR0200
          I = I + 1;                                                 PIKR0210
          IF (MK) THEN GO TO NDL;                                     ELSE;    PIKR0220
          IF (I = IACR+1) THEN GO TO FLS;                           ELSE GO TO SGD;
FLS:      I = 0;                                                    PIKR0230
          MK = '1'B;                                                 PIKR0240
          GO TO SGD;                                                 PIKR0250
          RETURN;                                                    PIKR0260
NDL:      END PICKER;                                               PIKR0270
                                                PIKR0280

```

```

* PROCESS('ATR,XREF,NOSTMT,OPT=02');                                NRLY0010
/* PICK PEAKS BETWEEN LAYERS AND OUTPUT THEIR POSITION AND HEIGHT */ NRLY0020
NTRLAY:  PROCEDURE (IACR,IDWN,ILAY,FW,SP,IACS,PMIN,PMAX,#PEAK,IPRT); NRLY0030
        DECLARE (IACR,IDWN,ILAY,FW,SP,IACS,PMIN,PMAX,#PEAK,IPRT)
        FIXED BINARY (15);                                          NRLY0040
        DECLARE (LAYER(0:IACR,0:IDWN), LYRB4(0:IACR,0:IDWN))
        CONTROLLED FIXED BINARY (15);                               NRLY0060
        DECLARE HEAD
        DECLARE 1 PEAK,                                             NRLY0070
        2 (U,V,W,VALU)      FIXED BINARY (31);                     NRLY0080
        DECLARE MPOUT      FILE ENVIRONMENT(REGIONAL(1)) KEYED,   NRLY0090
        PEAKS              FILE RECORD SEQUENTIAL;                NRLY0100
        DECLARE LNACR(0:IACR)   CONTROLLED FIXED BINARY(15);      NRLY0110
        ALLOCATE LNACR;                                             NRLY0120
        #PEAK = 0;                                                 NRLY0130
        PUT PAGE;                                                 NRLY0140
        OPEN FILE (MPOUT) UPDATE RECORD DIRECT;                   NRLY0150
        ALLOCATE LAYER, LYRB4;                                     NRLY0160
        READ FILE (MPOUT) INTO (LYRB4) KEY (ILAY-1);              NRLY0170
/*
        GO THROUGH THE MAP LAYER BY LAYER                          NRLY0180
                                                                NRLY0190
                                                                NRLY0200
                                                                NRLY0210
                                                                */
LAYLUP:  DO L = 0 TO ILAY-1 BY 1;                                    NRLY0220
        READ FILE (MPOUT) INTO (LAYER) KEY(L);                    NRLY0230
        IF (L=0) THEN LB4 = ILAY - 1;                              NRLY0240
        ELSE LB4 = L - 1;                                          NRLY0250
                                                                NRLY0260
                                                                NRLY0270
                                                                NRLY0280
                                                                */
/*
        GO THROUGH EACH LAYER LINE BY LINE                          NRLY0290
                                                                NRLY0300
                                                                NRLY0310
                                                                NRLY0320
                                                                NRLY0330
                                                                NRLY0340
                                                                NRLY0350
DWNLUP:  DO K = 0 TO IDWN BY 1;
        IF (K=0) THEN IDM = IDWN - 1;
        ELSE IDM = K - 1;
        IF (K=IDWN) THEN IDP = 1;
        ELSE IDP = K + 1;
/*

```

```

GO THROUGH EACH LINE POINT BY POINT
ACRLUP: DO J = 0 TO IACR BY 1;
IF (LAYER(J,K) = 0) THEN GO TO NDAL;
IF (J=0) THEN IAM = IACR - 1;
ELSE IAM = J - 1;
IF (J=IACR) THEN IAP = 1;
ELSE IAP = J + 1;
LJK = LAYER(J,K);
LAJK = ABS(LAYER(J,K));
/*
DETERMINE IF THE PEAK SHOULD BE KEPT
IF (ABS(LYRB4(IAP, IDP)) > LAJK) THEN LJK = -LAJK;
ELSE LYRB4(IAP, IDP) = -ABS(LYRB4(IAP, IDP));
IF (ABS(LYRB4(IAP, K)) > LAJK) THEN LJK = -LAJK;
ELSE LYRB4(IAP, K) = -ABS(LYRB4(IAP, K));
IF (ABS(LYRB4(IAP, IDM)) > LAJK) THEN LJK = -LAJK;
ELSE LYRB4(IAP, IDM) = -ABS(LYRB4(IAP, IDM));
IF (ABS(LYRB4(J, IDP)) > LAJK) THEN LJK = -LAJK;
ELSE LYRB4(J, IDP) = -ABS(LYRB4(J, IDP));
IF (ABS(LYRB4(J, K)) > LAJK) THEN LJK = -LAJK;
ELSE LYRB4(J, K) = -ABS(LYRB4(J, K));
IF (ABS(LYRB4(J, IDM)) > LAJK) THEN LJK = -LAJK;
ELSE LYRB4(J, IDM) = -ABS(LYRB4(J, IDM));
IF (ABS(LYRB4(IAM, IDP)) > LAJK) THEN LJK = -LAJK;
ELSE LYRB4(IAM, IDP) = -ABS(LYRB4(IAM, IDP));
IF (ABS(LYRB4(IAM, K)) > LAJK) THEN LJK = -LAJK;
ELSE LYRB4(IAM, K) = -ABS(LYRB4(IAM, K));
IF (ABS(LYRB4(IAM, IDM)) > LAJK) THEN LJK = -LAJK;
ELSE LYRB4(IAM, IDM) = -ABS(LYRB4(IAM, IDM));
LAYER(J,K) = LJK;
NDAL: END ACRLUP;
END DOWNLUP;
REWRITE FILE (MPOUT) FROM (LYRB4) KEY (LB4);
IF (IPRT=1) THEN CALL OUTP;
PUT EDIT ('MAP LAYER ',L,' HAS BEEN REWRITTEN')
(SKIP,A,F(3),A);
LYRB4 = LAYER;
END LAYLUP;
REWRITE FILE (MPOUT) FROM (LAYER) KEY (ILAY-1);
FREE LYRB4;
PUT PAGE;
OPEN FILE (PEAKS) OUTPUT;
/*
FIND AND WRITE OUT ALL THE PEAKS
LUPLAY: DO L = 0 TO ILAY-1 BY 1;
READ FILE (MPOUT) INTO (LAYER) KEY (L);
W = L;

```

```

NRLY0360
*/ NRLY0370
NRLY0380
ELSE; NRLY0390
NRLY0400
NRLY0410
NRLY0420
NRLY0430
NRLY0440
NRLY0450
NRLY0460
NRLY0470
*/ NRLY0480
NRLY0490
NRLY0500
NRLY0510
NRLY0520
NRLY0530
NRLY0540
NRLY0550
NRLY0560
NRLY0570
NRLY0580
NRLY0590
NRLY0600
NRLY0610
NRLY0620
NRLY0630
NRLY0640
NRLY0650
NRLY0660
NRLY0670
NRLY0680
NRLY0690
NRLY0700
ELSE; NRLY0710
NRLY0720
NRLY0730
NRLY0740
NRLY0750
NRLY0760
NRLY0770
NRLY0780
NRLY0790
NRLY0800
NRLY0810
*/ NRLY0820
NRLY0830
NRLY0840
NRLY0850

```



```

REV3:  T = B(IJ);
        IF (B.EG(I) >= T.EG) THEN      GO TO L40;      ELSE;      PKST0620
        B(IJ) = B(I);                  PKST0630
        B(I) = T;                        PKST0640
        T = B(IJ);                       GO TO L40;      PKST0650
L30:   B(L) = B(K);                      PKST0660
        B(K) = TT;                       PKST0670
L40:   L = L-1;                           PKST0680
REV4:  IF (B.EG(L) < T.EG) THEN          GO TO L40;      ELSE;      PKST0690
        TT = B(L);                       PKST0700
L50:   K = K+1;                           PKST0710
REV5:  IF (B.EG(K) > T.EG) THEN          GO TO L50;      ELSE;      PKST0720
        IF (K <= L) THEN                 GO TO L30;      ELSE;      PKST0730
        IF (L-I <= J-K) THEN             GO TO L60;      ELSE;      PKST0740
        IL(M) = I;                       PKST0750
        IU(M) = L;                       PKST0760
        I = K;                            PKST0770
        M = M+1;                          GO TO L80;      PKST0780
L60:   IL(M) = K;                         PKST0790
        IU(M) = J;                       PKST0800
        J = L;                            PKST0810
0.615661 M = M+1;                        GO TO L80;      PKST0820
L70:   M = M-1;                           PKST0830
        IF (M = 0) THEN GO TO NDSRT;      ELSE;      PKST0840
        I = IL(M);                       PKST0850
        J = IU(M);                       PKST0860
L80:   IF (J-I >= II) THEN               GO TO L10;      ELSE;      PKST0870
        IF (I = II) THEN                 GO TO L05;      ELSE;      PKST0880
        I = I-1;                          PKST0890
L90:   I = I+1;                          PKST0900
        IF (I = J) THEN                  GO TO L70;      ELSE;      PKST0910
        T = B(I+1);                      PKST0920
REV6:  IF (B.EG(I) >= T.EG) THEN          GO TO L90;      ELSE;      PKST0930
        K = I;                            PKST0940
L95:   B(K+1) = B(K);                    PKST0950
        K = K-1;                          PKST0960
REV7:  IF (T.EG > B.EG(K)) THEN          GO TO L95;      ELSE;      PKST0970
        B(K+1) = T;                      GO TO L90;      PKST0980
/*                                         PKST0990
        WRITE OUT THE SORTED PEAKS      PKST1000
                                           PKST1010
                                           PKST1020
                                           */
NDSRT: PUT EDIT ('LIST OF SORTED PEAKS',
               '      IU      IV      IW      IHEIGHT      ',
               '      IU      IV      IW      IHEIGHT      ',
               '      IU      IV      IW      IHEIGHT      ',
               (PAGE,A,SKIP,3 A));
        PUT SKIP;
LUP1:  OPEN FILE (PEAKS) OUTPUT;
        DO I = 1 TO #PEAK BY 1;
        PEAK.U = B.U(I);

```

```

PEAK.V = B.V(I);
PEAK.W = B.W(I);
PEAK.VALU = B.EG(I);
WRITE FILE (PEAKS) FROM (PEAK);
PUT EDIT (PEAK,' ') (4 F(10),X(3),A);
PUT FILE (PUNCH) EDIT (PEAK) (4 F(5));
END LUPI;
CLOSE FILE (PEAKS);
FREE B;
PUT EDIT ('THE SORTED PEAKS HAVE BEEN WRITTEN OUT')
      (SKIP(4),A);
RETURN;
END PKSORT;

```

```

PKST1120
PKST1130
PKST1140
PKST1150
PKST1160
PKST1170
PKST1180
PKST1190
PKST1200
PKST1210
PKST1220
PKST1230
PKST1240

```

```

* PROCESS('ATR,XREF');
/* PROCEDURE TO PRINT A LINE OF THE MAP
(SUBRG,STRG):
PLINE: PROCEDURE (FW, SP, PMN, PMX, LN, ACRS, ACRE, LIN);
      DECLARE NUMS(*) CHAR(*) EXTERNAL CONTROLLED,
      HEAD CHAR (132) STATIC EXTERNAL,
      LINE CHAR (132) STATIC,
      LIN(*) CONTROLLED FIXED BINARY,
      (FW, SP, PMN, PMX, LN, ACRS, ACRE, LL)
      FIXED BINARY;

      LINE = HEAD;
      SUBSTR(LINE,1,2) = SUBSTR(NUMS(LN),FW-1,2);
      J = 5 - FW;
LOOP: DO I = ACRS TO ACRE;
      J = J + FW;
      LL = LIN(I);
      IF (LL < PMN) THEN LL = PMN - 1;
      IF (LL > PMX) THEN LL = PMX + 1;
      SUBSTR(LINE,J,FW) = NUMS(LL);
      J = J + FW + 2;
      IF (J > 130) THEN GO TO PRINT;
      SUBSTR(LINE,J,2) = SUBSTR(NUMS(LN),FW-1,2);
PRINT: PUT SKIP(SP+1) EDIT (LINE) (A(132));
      RETURN;
      END PLINE;
      END LOOP;

```

```

*/
PLIN0010
PLIN0020
PLIN0030
PLIN0040
PLIN0050
PLIN0060
PLIN0070
PLIN0080
PLIN0090
PLIN0200
PLIN0210
PLIN0220
PLIN0230
PLIN0240
PLIN0250
PLIN0260
PLIN0270
PLIN0280
PLIN0290
PLIN0300
PLIN0310
PLIN0320
PLIN0330
PLIN0340
PLIN0350

```

```

//LKED.SYSLMOD DD DSNAME=PROG.CRYST,
// UNIT=DISK,VOLUME=SER=PROGPK,DISP=(OLD,KEEP)
//LKED.SYSIN DD *
OVERLAY ALPHA

```

```

JCL-0060
JCL-0070
JCL-0080
OVLY0010

```

INSERT SETUP
OVERLAY BETA
INSERT TM_DT
OVERLAY BETA
INSERT PRSETUP
OVERLAY ALPHA
INSERT LAYERS
INSERT PICKER
OVERLAY ALPHA
INSERT NTRLAY
INSERT PLINE
OVERLAY ALPHA
INSERT PKSORT
NAME ALPP(R)

OVLY0020
OVLY0030
OVLY0040
OVLY0050
OVLY0060
OVLY0070
OVLY0080
OVLY0090
OVLY0100
OVLY0110
OVLY0120
OVLY0130
OVLY0140
JCL-0090

APPENDIX B

PROGRAM LISTING OF ALOP


```

DECLARE STAMP CHARACTER (54) EXTERNAL; ALPO0460
DECLARE 1 SYMMPQ (#SYMM) CONTROLLED EXTERNAL, ALPO0470
2 (PX,QX,PY,QY,PZ,QZ) FIXED BINARY (15); ALPO0480
DECLARE (#PEAKS,#SYMM,#RTND,IACR,IDWN,ILAY) ALPO0490
FIXED BINARY (15); ALPO0500
DECLARE (SGNL, NCNT) BIT (1) EXTERNAL; ALPO0510
ALPO0520
/*
SGNL='1'B IF THERE IS A SYMMETRY ELEMENT WITH PX=PY=PZ=-1. ALPO0530
NCNT='1'B IF THERE ARE SYMMETRY ELEMENTS WITH ONLY: PX=-1, ALPO0540
PY=-1, PZ=-1, PX=PY=-1, PY=PZ=-1, PZ=PX=-1. ALPO0550
*/
DECLARE (ITXYZ,LNG,IERR) FIXED BINARY (31); ALPO0560
DECLARE IHESRTA ENTRY ((CHAR(53), CHAR(39), ALPO0570
FIXED BIN(31), FIXED BIN(31)); ALPO0580
DECLARE SFLD CHARACTER (53); ALPO0590
RFLD CHARACTER (39); ALPO0600
DECLARE SORTIN FILE RECORD SEQUENTIAL; ALPO0610
DECLARE SDBG CHARACTER (100) VARYING; ALPO0620
DECLARE DBG EXTERNAL BIT (1); ALPO0630
DECLARE DNV BIT (1) EXTERNAL; ALPO0640
IF (LENGTH(SDBG) > 1) THEN DNV = '1'B; ELSE DNV = '0'B; ALPO0650
IF (LENGTH(SDBG) = 0) THEN DBG = '0'B; ELSE DBG = '1'B; ALPO0660
CALL TM_DT; ALPO0670
LNG = 24000; ALPO0680
RFLD=' RECORD TYPE=V,LENGTH=(24,24,24,24,24) ' ; ALPO0690
ON SUBSCRIPTRANGE SNAP BEGIN; PUT DATA (I); EXIT; END; ALPO0700
ALPO0710
/*
READ AND INTERPRET THE CONTROL CARDS ALPO0720
IF (DBG) THEN PUT EDIT ('DEBUGGING OUTPUT WILL BE PRINTED.') ALPO0730
(SKIP(4),A); ELSE; ALPO0740
ALPO0750
GET EDIT (TITLE,#PEAKS,IACR,IDWN,ILAY,#SYMM) ALPO0760
(A(80),5 F(4)); ALPO0770
PUT EDIT (TITLE, STAMP, ALPO0780
'NUMBER OF POINTS ACROSS A FULL LINE =',IACR, ALPO0790
'NUMBER OF LINES DOWN A FULL LAYER =',IDWN, ALPO0800
'NUMBER OF LAYERS IN A FULL MAP =',ILAY, ALPO0810
'NUMBER OF PEAKS IN INPUT DATA SET =',#PEAKS, ALPO0820
'NUMBER OF SYMMETRY CARDS TO BE READ =',#SYMM) ALPO0830
(A(80),SKIP(3),A(54),5 (SKIP(3),X(20),A,F(4))); ALPO0840
ALPO0850
ALLOCATE SYMMPQ; ALPO0860
DO I = 1 TO #SYMM BY 1; ALPO0870
GET EDIT (PX(I),QX(I),PY(I),QY(I),PZ(I),QZ(I)) ALPO0880
(SKIP,6 F(4)); ALPO0890
PUT EDIT ('SYMMETRY OPERATION',I,PX(I),'*X +',QX(I),' /2', ALPO0900
PY(I),'*Y +',QY(I),' /2',PZ(I),'*Z +',QZ(I),' /2') ALPO0910
(SKIP(2),X(25),A,F(3),3 (F(7),A,F(2),A)); ALPO0920
ALPO0930
END SLUP; ALPO0940
GET SKIP; ALPO0950
/*

```

```

CLOSE FILE (SYSIN);
PICK AN APPROPRIATE HEAVY-ATOM PEAK & TEST ALL OTHER PEAKS
/* CALL PART1 (#PEAKS,IACR,IDWN,ILAY,#RTND);
USING SYMMETRY, FIND ALL POSSIBLE VALUES OF TX, TY, TZ
/* CALL PART2 (#RTND,IACR,IDWN,ILAY,#SYMM);
IF (-SGNL) THEN GO TO PT4;
/*
/* GROUP ALL TX, TY, TZ AND OUTPUT THOSE WITH FREQUENCY > 5
PT3: OPEN FILE (SORTIN) OUTPUT;
CALL PART3 (IACR,IDWN,ILAY,#RTND);
IF (-NCNT) THEN GO TO SRT;
/* PICK ALL NON-INVERSION TX,TY,TZ > 5 IN # AND OUTPUT W/ SYM#
PT4: CALL PART4 (IACR, IDWN, ILAY);
/* SORT THE FILE OF TX,TY,TZ BY TX, TY, TZ & SYM#
SRT: CLOSE FILE (SORTIN);
SFLD=' SORT FIELDS=(11,02,FI,D,21,4,FL,D),SIZE=E7000
CALL IHESRTA (SFLD,RFLD,LNG,IERR);
IF (IERR=0) THEN GO TO PT5;
PUT EDIT ('THE SECOND SORT WAS UNSUCCESSFUL -- RETRY')
(SKIP(2),A);
/* EXIT;
MAP THE SYMMETRY ELEMENTS INTO EACH OTHER
PT5: CALL PART5 (IACR, IDWN, ILAY);
/* CHOOSE THE MOST FREQUENT VALUE OF TX, TY, AND TZ
/* CALL PART6 (IACR, IDWN, ILAY);
/* DETERMINE WHICH PEAKS ARE TO BE KEPT
/* CALL PART7 (IACR, IDWN, ILAY, #RTND, #SYMM);
END ALOP;

* PROCESS('ATR,XREF,NOSTMT,OPT=02');
/* CREATES A TIME - DATE STAMP FOR FUTURE USE
(SUBRG,STRG): TM_DT: PROCEDURE;

```

```

ALP00960
ALP00970
*/ ALP00980
ALP00990
ALP01000
ALP01010
*/ ALP01020
ALP01030
ELSE; ALP01040
ALP01050
ALP01060
ALP01070
*/ ALP01080
ALP01090
ALP01100
ELSE; ALP01110
ALP01120
ALP01130
*/ ALP01140
ALP01150
ALP01160
ALP01170
*/ ALP01180
ALP01190
; ALP01200
ALP01210
ELSE; ALP01220
ALP01230
ALP01240
ALP01250
ALP01260
*/ ALP01270
ALP01280
ALP01290
ALP01300
*/ ALP01310
ALP01320
ALP01330
ALP01340
ALP01350
*/ ALP01360
ALP01370
ALP01380

TMDT0010
*/ TMDT0020
TMDT0030

```

```

DECLARE STAMP CHARACTER(54) EXTERNAL, AMPM CHARACTER(4);
DECLARE MOS(12) CHARACTER(9) VARYING, INITIAL ('JANUARY', 'FEBRUARY',
'MARCH', 'APRIL', 'MAY', 'JUNE', 'JULY', 'AUGUST', 'SEPTEMBER',
'OCTOBER', 'NOVEMBER', 'DECEMBER');
DECLARE TM CHARACTER(9), TMS(2) CHARACTER(2) DEFINED TM; TM = TIME;
DECLARE DT CHARACTER(6), DS(3) CHARACTER(1) ELSE AMPM = 'A.M.'; DT = DATE;
IF (TMS(1) > 11) THEN AMPM = 'P.M.'; !! DS(3) !! DS(1) !!
STAMP = 'RUN ON ' || MOS(OS(2)) || ' HOURS ' || TMS(2) || ' AMPM;
' AT ' || TMS(1) || ' MINUTES ' || AMPM;
END TM_DT;

```

```

TMDT0040
TMDT0050
TMDT0060
TMDT0070
TMDT0080
TMDT0090
TMDT0100
TMDT0110
TMDT0120
TMDT0130

```

```

* PROCESS( 'ATR, XREF, NDSTMT, OPT=02' );
/* PICK AN APPROPRIATE HEAVY-ATOM PEAK & TEST ALL OTHER PEAKS */
/* IN-CORE HEAVY-ATOM SINGLE SUPERPOSITION */
PART1:
PROCEDURE (#PEAKS, IACR, IDWN, ILAY, #RTND); FIXED BINARY (15);
DECLARE 1 PEAKS (#PEAKS) CONTROLLED;
DECLARE 2 (U, V, W, VALU, MEAN) FIXED BINARY (15);
DECLARE PKFILE
DECLARE RETAIN
DECLARE 1 PEAKR;
DECLARE 1 2 (RU, RV, RW, VAL, AVG) FIXED BINARY (31);
DECLARE 1 2 (SU, SV, SW, VLU) FIXED BINARY (31);
DECLARE DIF
DECLARE (BU, BV, BW)
DECLARE (DELU, DELV, DELW)
DECLARE (P1, P2, P3)
DECLARE (IDU, IDV, IDW)
DECLARE DBG
ON SUBSCRIPT RANGE SNAP BEGIN;
PUT DATA (I, J, K, L); EXIT; END;
SET UP CONSTANTS FOR CHECKING
IA2 = IACR / 2;
ID2 = IDWN / 2;
IL2 = ILAY / 2;
P1 = 0.800;
P2 = 0.650;
P3 = 0.500;
/* READ IN THE PEAKS PICKED FROM THE MAP BY ALPPKR
ALLOCATE PEAKS;
DO I = 1 TO #PEAKS BY 1;
GET EDIT (SPEAK) {4 F(5)};
U(I) = SU;
*/
PI-0010
PI-0020
PI-0030
PI-0040
PI-0050
PI-0060
PI-0070
PI-0080
PI-0090
PI-0100
PI-0110
PI-0120
PI-0130
PI-0140
PI-0150
PI-0160
PI-0170
PI-0180
PI-0190
PI-0200
PI-0210
PI-0220
PI-0230
PI-0240
PI-0250
PI-0260
PI-0270
PI-0280
PI-0290
PI-0300
PI-0310
PI-0320
PI-0330
PI-0340
PI-0350
PI-0360

```



```

V(I) = SV;
W(I) = SW;
VALU(I) = VLU;
MEAN(I) = 0;
END PLUP;
/*
FIND THE LIKELY HEAVY ATOM PEAK FROM THE FIRST 20%
IF (#PEAKS<100) THEN ITOP = MIN(20,#PEAKS);
ELSE ITOP = #PEAKS / 5;
IA2 = IACR / 2;
ID2 = IDWN / 2;
IL2 = ILAY / 2;
DIF = HARD;
ITIME = 1;
JTIME = 0;
DO I = 1 TO ITOP BY 1;
  IU = U(I);
  IV = V(I);
  IW = W(I);
  KVAL = VALU(I);
  GO TO DIF;
/*
LARGEST PEAK ACCEPTED AS HEAVY ATOM WHICH HASN'T U,V,W=0,1/2
IF ((IU=0)|(IV=IACR)|(IU=IA2)|(IV=0)|(IV=IDWN)|(IV=ID2)|
  (IW=0)|(IW=ILAY)|(IW=IL2)) THEN GO TO NOPE;
ELSE GO TO YEP;
/*
LARGEST ACCEPTED AS HEAVY ATOM HAVING ONLY ONE OF U,V,W=0,1/2
BU = ~((IU=0)|(IV=IACR)|(IU=IA2));
BV = ~((IV=0)|(IV=IDWN)|(IV=ID2));
BW = ~((IW=0)|(IW=ILAY)|(IW=IL2));
IF (BU&BV) | (BU&BW) | (BV&BW) THEN GO TO YEP;
ELSE GO TO NOPE;
/*
LARGEST ACCEPTED AS HEAVY ATOM HAVING TWO ONLY OF U,V,W=0,1/2
BU = ~((IU=0)|(IV=IACR)|(IU=IA2));
BV = ~((IV=0)|(IV=IDWN)|(IV=ID2));
BW = ~((IW=0)|(IW=ILAY)|(IW=IL2));
IF (BU | BV | BW) THEN GO TO YEP;
ELSE GO TO NOPE;
NOPE:
END TLUP;
IF (ITIME=1) THEN GO TO FIRST;
ELSE IF (ITIME=2) THEN GO TO SCND;
ELSE GO TO FAIL;
FIRST:
DIF = MEDM;
ITIME = 2;

```

--P1-0370
--P1-0380
--P1-0390
--P1-0400
--P1-0410
--P1-0420
--P1-0430
--P1-0440
--P1-0450
--P1-0460
--P1-0470
--P1-0480
--P1-0490
--P1-0500
--P1-0510
--P1-0520
--P1-0530
--P1-0540
--P1-0550
--P1-0560
--P1-0570
--P1-0580
--P1-0590
--P1-0600
--P1-0610
--P1-0620
--P1-0630
--P1-0640
--P1-0650
--P1-0660
--P1-0670
--P1-0680
--P1-0690
--P1-0700
--P1-0710
--P1-0720
--P1-0730
--P1-0740
--P1-0750
--P1-0760
--P1-0770
--P1-0780
--P1-0790
--P1-0800
--P1-0810
--P1-0820
--P1-0830
--P1-0840
--P1-0850
--P1-0860

```

SCND:  GO TO TLUP;                                -P1-0870
        DIF = EASY;                                -P1-0880
        ITIME = 3;                                 -P1-0890
        GO TO TLUP;                                -P1-0900
/*
        UNABLE TO FIND A SUITABLE HEAVY ATOM      -P1-0910
*/
FAIL:  PUT EDIT ('***** UNABLE TO PICK A HEAVY-ATOM PEAK *****') -P1-0920
        (SKIP(4),A);                               */ -P1-0930
        EXIT;                                      -P1-0940
/*
        SUITABLE HEAVY ATOM PEAK FOUND           -P1-0950
*/
YEP:   KU = IU;                                    -P1-0960
        KV = IV;                                    -P1-0970
        KW = IW;                                    -P1-0980
        KP = I;                                      -P1-0990
        PUT EDIT ('HEAVY ATOM PEAK FOUND AT U =',KU,'V =',KV,'W =', -P1-1000
                 KW,'VALUE =',KVAL)                -P1-1010
                 (SKIP(3),X(20), 4 (A,F(4),X(3))); -P1-1020
/*
        DECIDE ON WHETHER TO USE A HARKER OR A GENERAL PEAK -P1-1030
*/
        IF ((ITIME=1) & (JTIME=0)) THEN GO TO TAGN; ELSE; -P1-1040
        IF ((ITIME=1) & (JTIME=1)) THEN GO TO COMPR; ELSE; -P1-1050
TAGN:  GO TO RSTR;                                  -P1-1060
        GKP = KP;          GKVL = KVAL;          JTIME = 1; -P1-1070
        GKU = KU;          GKV = KV;            GKW = KW; -P1-1080
        GO TO FIRST;                                  -P1-1090
COMPR: GNRL = FLOAT (GKVL);                          -P1-1100
        HRKR = FLOAT (KVAL) / 2.2000;                -P1-1110
        IF (HRKR > GNRL) THEN GO TO TYPE;            ELSE; -P1-1120
        KU = GKU;          KV = GKV;          KW = GKW; -P1-1130
        KP = GKP;          KVAL = GKVL;            -P1-1140
TYPE:  PUT EDIT ('#### PEAK FINALLY CHOSEN AT:  ####', -P1-1150
                 'U =',KU,'V =',KV,'W =',KW,'VALUE =',KVAL, -P1-1160
                 'INDEX =',KP) (SKIP(2),X(10),A,SKIP,3 (X(20),A,F(5)), -P1-1170
                 SKIP,2 (X(20),A,F(5)));            -P1-1180
/*
        USING THIS PEAK, DETERMINE WHICH PEAKS TO RETAIN -P1-1190
*/
RSTR:  PUT EDIT ('PEAKS FOUND, USING HEAVY-ATOM PEAK', -P1-1200
                 '      U      V      W      HEIGHT      MEAN', -P1-1210
                 '      U      V      W      HEIGHT      MEAN', -P1-1220
                 '      U      V      W      HEIGHT      MEAN', -P1-1230
                 '      U      V      W      HEIGHT      MEAN', -P1-1240
                 (PAGE,A,SKIP,A,A,A,A,SKIP,A)); -P1-1250
        PUT SKIP;                                     -P1-1260
        DO I = 1 TO #PEAKS BY 1;                      -P1-1270
/*
        ILUP:
*/

```

```

CALCULATE THE PEAK POSITION TO LOOK FOR
                                                                    */
K = I;
IDU = KU + U(I);
IDV = KV + V(I);
IDW = KW + W(I);
IF (IDU<0) THEN IDU = IDU + IACR;
ELSE IF (IDU>IACR) THEN IDU = IDU - IACR; ELSE;
IF (IDU<0) THEN IDU = IDU + IACR;
ELSE IF (IDU>IACR) THEN IDU = IDU - IACR; ELSE;
IF (IDV<0) THEN IDV = IDV + IDWN;
ELSE IF (IDV>IDWN) THEN IDV = IDV - IDWN; ELSE;
IF (IDV<0) THEN IDV = IDV + IDWN;
ELSE IF (IDV>IDWN) THEN IDV = IDV - IDWN; ELSE;
IF (IDW<0) THEN IDW = IDW + ILAY;
ELSE IF (IDW>ILAY) THEN IDW = IDW - ILAY; ELSE;
IF (IDW<0) THEN IDW = IDW + ILAY;
ELSE IF (IDW>ILAY) THEN IDW = IDW - ILAY; ELSE;

/*
DETERMINE IF ANY OF THE OTHER PEAKS FITS EXACTLY
TO THIS CALCULATED POSITION, OR IF IT IS OFF ONLY SLIGHTLY
                                                                    */
JLUP: DO J = 1 TO #PEAKS BY 1;
L = J;
DELU = U(J) - IDU;
DELV = V(J) - IDV;
DELW = W(J) - IDW;
IF (DELU > IA2) THEN DELU = DELU - IACR; ELSE;
IF (DELU > IA2) THEN DELU = DELU - IACR; ELSE;
IF (DELU < -IA2) THEN DELU = DELU + IACR; ELSE;
IF (DELU < -IA2) THEN DELU = DELU + IACR; ELSE;
IF (DELV > ID2) THEN DELV = DELV - IDWN; ELSE;
IF (DELV > ID2) THEN DELV = DELV - IDWN; ELSE;
IF (DELV < -ID2) THEN DELV = DELV + IDWN; ELSE;
IF (DELV < -ID2) THEN DELV = DELV + IDWN; ELSE;
IF (DELW > IL2) THEN DELW = DELW - ILAY; ELSE;
IF (DELW > IL2) THEN DELW = DELW - ILAY; ELSE;
IF (DELW < -IL2) THEN DELW = DELW + ILAY; ELSE;
IF (DELW < -IL2) THEN DELW = DELW + ILAY; ELSE;
IF ((DELU=0) & (DELV=0) & (DELW=0)) THEN GO TO OFF0; ELSE;
DELU = ABS (DELU);
DELV = ABS (DELV);
DELW = ABS (DELW);
IF ( ((DELU=1) & (DELV=0) & (DELW=0)) |
      ((DELU=0) & (DELV=1) & (DELW=0)) |
      ((DELU=0) & (DELV=0) & (DELW=1)) ) THEN GO TO OFF1; ELSE;
IF ( ((DELU=1) & (DELV=1) & (DELW=0)) |
      ((DELU=0) & (DELV=1) & (DELW=1)) |
      ((DELU=1) & (DELV=0) & (DELW=1)) ) THEN GO TO OFF2; ELSE;
IF ((DELU=1) & (DELV=1) & (DELW=1)) THEN GO TO OFF3; ELSE;

```

```

END JLUP;
GO TC NDI;

/*
PEAK IS RIGHT ON
MEAN(J) = SQRT (FLOAT (VALU(I) * VALU(J)));
PUT EDIT (U(J),V(J),W(J),VALU(J),MEAN(J)) (3 F(5),2 F(9));
GO TO NDI;
*/

PEAK IS OFF 1 GRID IN ONE DIRECTION
MEAN(J) = P1 * SQRT (FLOAT (VALU(I) * VALU(J)));
PUT EDIT (U(J),V(J),W(J),VALU(J),MEAN(J)) (3 F(5),2 F(9));
GO TC NDI;
*/

THE PEAK IS OFF 1 GRID POINT IN EACH OF TWO DIRECTIONS
MEAN(J) = P2 * SQRT (FLOAT (VALU(I) * VALU(J)));
PUT EDIT (U(J),V(J),W(J),VALU(J),MEAN(J)) (3 F(5),2 F(9));
GO TO NDI;
*/

THE PEAK IS OFF 1 GRID POINT IN ALL THREE DIRECTIONS
MEAN(J) = P3 * SQRT (FLOAT (VALU(I) * VALU(J)));
PUT EDIT (U(J),V(J),W(J),VALU(J),MEAN(J)) (3 F(5),2 F(9));
END ILUP;
*/

WRITE OUT THE PEAKS WHICH WERE FOUND
OPEN FILE (RETAIN) OUTPUT;
#RTND = 0;
DO I = 1 TO #PEAKS BY 1;
IF (MEAN(I)=0) THEN GO TO FNLI;
RU = U(I);
RV = V(I);
RW = W(I);
VAL = VALU(I);
AVG = MEAN(I);
#RTND = #RTND + 1;
WRITE FILE (RETAIN) FROM (PEAKR);
END LUPI;
CLOSE FILE (RETAIN);
FREE PEAKS;
RETURN;
END PART I;

FNLI:

LUPI:
ELSE;

/*
PROCESS('ATR,XREF,NOSTMT,OPT=02');

```

```

-PI-1870
-PI-1880
-PI-1890
-PI-1900
-PI-1910
-PI-1920
-PI-1930
-PI-1940
-PI-1950
-PI-1960
-PI-1970
-PI-1980
-PI-1990
-PI-2000
-PI-2010
-PI-2020
-PI-2030
-PI-2040
-PI-2050
-PI-2060
-PI-2070
-PI-2080
-PI-2090
-PI-2100
-PI-2110
-PI-2120
-PI-2130
-PI-2140
-PI-2150
-PI-2160
-PI-2170
-PI-2180
-PI-2190
-PI-2200
-PI-2210
-PI-2220
-PI-2230
-PI-2240
-PI-2250
-PI-2260
-PI-2270
-PI-2280
-PI-2290
-PI-2300
-PI-2310

```

-P2-0010

```

/* USING SYMMETRY, FIND ALL THE VALUES OF TX, TY, TZ          */ -P2-0020
/* FROM THE PEAKS OBTAINED FROM THE SUPERPOSITION OF PART 1   */ -P2-0030
PART2:  PROCEDURE (#RTND,IACR,IOWN,ILAY,#SYMM);                -P2-0040
/*                                                              -P2-0050

```

```

THIS SECTION COMPUTES ALL OF THE POSSIBLE VALUES OF TX, TY, & -P2-0060
TZ FROM THE PEAKS LEFT BY THE SUPERPOSITION AS FOLLOWS:      -P2-0070
LET U, V, W & U', V', W' REPRESENT THE TWO PEAKS. IF THESE PEAKS -P2-0080
ARE SYMMETRY RELATED BUT THE SUPERPOSITION ORIGIN IS OFF     -P2-0090
BY TX, TY, TZ, THEN U = X+TX, V = Y+TY, AND W = Z+TZ. DEPENDING -P2-0100
ON THE VALUES OF PX, PY, PZ THERE ARE THEN 18 DIFFERENT COMBINA--P2-0110
TIONS OF THE TWO PEAKS (DESIGNATED AS P1 AND P2):            -P2-0120

```

QUANTITY	U OF QUANTITY	V OF QUANTITY	W OF QUANTITY	
P1	X + TX	Y + TY	Z + TZ	-P2-0130
P2(0)	QX + X + TX	QY + Y + TY	QZ + Z + TZ	-P2-0140
P2(0)+P1	QX + 2X + 2TX	QY + 2Y + 2TY	QZ + 2Z + TZ	-P2-0150
P2(0)-P1	QX	QY	QZ	-P2-0160
P2(1)	QX - X + TX	QY + Y + TY	QZ + Z + TZ	-P2-0170
P2(1)+P1	* QX + 2TX	QY + 2Y + 2TY	QZ + 2Z + TZ	-P2-0180
P2(1)-P1	QX - 2X	# QY	# QZ	-P2-0190
P2(2)	QX + X + TX	QY - Y + TY	QZ + Z + TZ	-P2-0200
P2(2)+P1	QX + 2X + 2TX	* QY + 2TY	QZ + 2Z + 2TZ	-P2-0210
P2(2)-P1	# QX	QY - 2Y	# QZ	-P2-0220
P2(3)	QX - X + TX	QY - Y + TY	QZ + Z + TZ	-P2-0230
P2(3)+P1	* QX + 2TX	* QY + 2TY	QZ + 2Z + 2TZ	-P2-0240
P2(3)-P1	QX - 2X	QY - 2Y	# QZ	-P2-0250
P2(4)	QX + X + TX	QY + Y + TY	QZ - Z + TZ	-P2-0260
P2(4)+P1	QX + 2X + 2TX	QY + 2Y + 2TY	* QZ + 2TZ	-P2-0270
P2(4)-P1	# QX	# QY	QZ - 2Z	-P2-0280
P2(5)	QX - X + TX	QY + Y + TY	QZ - Z + TZ	-P2-0290
P2(5)+P1	* QX + 2TX	QY + 2Y + 2TY	* QZ + 2TZ	-P2-0300
P2(5)-P1	QX - 2X	# QY	QZ - 2Z	-P2-0310
P2(6)	QX + X + TX	QY - Y + TY	QZ - Z + TZ	-P2-0320
P2(6)+P1	QX + 2X + 2TX	* QY + 2TY	* QZ + 2TZ	-P2-0330
P2(6)-P1	# QX	QY - 2Y	QZ - 2Z	-P2-0340
P2(7)	QX - X + TX	QY - Y + TY	QZ - Z + TZ	-P2-0350
P2(7)+P1	* QX + 2TX	* QY + 2TY	* QZ + 2TZ	-P2-0360
P2(7)-P1	QX - 2X	QY - 2Y	QZ - 2Z	-P2-0370

```

AS QX, QY, QZ ARE EITHER 0 OR 1/2 FOR ANY SYMMETRY ELEMENT AND -P2-0400
ARE KNOWN, VALUES OF TX; TY; TX, TY; TZ; TX, TZ; TY, TZ OR -P2-0410
TX, TY, TZ ARE THEN COMPUTED. FOR ALL BUT THE INVERSION, THE -P2-0420
FREQUENCY OF OCCURRENCE OF THESE VALUES IS STORED IN CORE. -P2-0430
FOR THE INVERSION, THE TX, TY, TZ TRIPLES ARE WRITTEN OUT, -P2-0440
SORTED INTO ORDER, AND THEN GROUPED TOGETHER ON REAPING IN -P2-0450
PART 3. A LATITUDE OF ONE GRID POINT IN EACH DIRECTION IS -P2-0460
ALLOWED FOR THE VALUES OF TX, TY, TZ AND APPROPRIATE WEIGHTS -P2-0470
ASSIGNED. THE ASTERISKED (*) RELATIONS ABOVE GIVE VALUES -P2-0480
OF TX, TY, TZ, PROVIDED THE NUMBERED (#) RELATIONS ARE OBEYED. -P2-0490
-P2-0500
-P2-0510

```

```

/*
DECLARE (#RTND, IACR, IDWN, ILAY, #SYMM)    FIXED BINARY (15);
DECLARE IS (#SYMM)                          FIXED BINARY (15) CONTROLLED;
DECLARE 1 PEAKS (#RTND)                     CONTROLLED EXTERNAL;
DECLARE 2 (U, V, W, VALU, MEAN)             FIXED BINARY (15);
DECLARE 1 SYMPPQ (#SYMM)                   CONTROLLED EXTERNAL;
DECLARE 2 (PX, QX, PY, QY, PZ, QZ)         FIXED BINARY (15);
DECLARE 1 RETAIN                           FILE RECORD SEQUENTIAL;
DECLARE 1 PEAKR, (RU, RV, RW, VAL, AVG)     FIXED BINARY (31);
DECLARE 1 TXYZ, (TX, TY, TZ, KS)           FIXED BINARY (15);
DECLARE 2 (VIJ, MIJ, FREQ)                 FLOAT BINARY;
DECLARE SYM(7)                              LABEL;
DECLARE ITXYZ                               FIXED BINARY (31);
DECLARE (XLINE#(0: IACR), YLINE#(0: IDWN), ZLINE#(0: ILAY),
        XYLAY#(0: IA, 0: ID), YZLAY#(0: IL), ZXLAY#(0: IL, 0: IA))
        EXTERNAL CONTROLLED FLOAT BINARY;
        EXTERNAL SHOWS THE TYPE OF SYMMETRY
        THE SEVEN-MEMBERED BIT(1) ARRAY IS SET IF THE SYMMETRY ELEMENT IS
        PRESENT.
ELEMENT NO PX PY PZ DETERMINE TX, TY, TZ?
PLANE PERP. TO X 1 1 1 TX
PLANE PERP. TO Y 2 1 1 TY
PLANE IN Z 3 1 1 TZ
PLANE IN PERP. TO Z 4 1 1 TZ
AXIS IN Y 5 1 1 TZ
AXIS IN X 6 1 1 TZ
INVERSION 7 1 1 TZ
SGNL=I,B IF THERE IS AN INVERSION; NCNT='1'B IF THERE ARE OTHERS
/*
DECLARE (ION(7), SGNL, NCNT)               BIT (1) EXTERNAL;
DECLARE AL(7)                              LABEL;
DECLARE DBG                                 EXTERNAL BIT (1);
DECLARE (IA2, ID2, IL2, I4A, I4D, I4L, JPIU, JPIW, JMIU, JMIV,
        JMIW, JMIUP, JMIVP, JMIWP, JMIWM, JMIWM)
        FIXED BINARY (15);
DECLARE LAY# (0: ILAY)                     EXTERNAL CTL BIT(1);
DECLARE (XQ, YQ, ZQ)                       EXTERNAL FIXED BIN;
IA2 = IACR / 2;
ID2 = IDWN / 2;
IL2 = ILAY / 2;
I4A = IACR * 4;
I4D = IDWN * 4;
I4L = ILAY * 4;
I1 : MIRRORS AND PLANES RIGHT ON (TX|TY|TZ).
I2 : TWO-FOLDS OR SCREWS RIGHT ON (TX, TY|TZ, TZ|TX, TZ).
I3 : MIRRORS AND PLANES OFF ONE GRID POINT.
I4 : TWO-FOLDS OR SCREWS OFF ONE IN ONE DIRECTION.
*/

```

*/

/*

/*

```

--P2-0520
--P2-0530
--P2-0540
--P2-0550
--P2-0560
--P2-0570
--P2-0580
--P2-0590
--P2-0600
--P2-0610
--P2-0620
--P2-0630
--P2-0640
--P2-0650
--P2-0660
--P2-0670
--P2-0680
--P2-0690
--P2-0700
--P2-0710
--P2-0720
--P2-0730
--P2-0740
--P2-0750
--P2-0760
--P2-0770
--P2-0780
--P2-0790
--P2-0800
--P2-0810
--P2-0820
--P2-0830
--P2-0840
--P2-0850
--P2-0860
--P2-0870
--P2-0880
--P2-0890
--P2-0900
--P2-0910
--P2-0920
--P2-0930
--P2-0940
--P2-0950
--P2-0960
--P2-0970
--P2-0980
--P2-0990
--P2-1000
--P2-1010

```

```

16 : TWO-FOLDS OR SCREWS OFF ONE IN BOTH DIRECTIONS.
DECLARE (I1,I2,I3,I4,I5,I6,TH)          FLOAT BINARY;
DECLARE (J1,J2,J3,J4,J5,J6,MEANIJ)     FLOAT BINARY;
TH = 10.000;                            J1 = 18;
J2 = 10;                                J3 = 9;
J4 = 6;                                  J5 = 4;
J6 = 2;
ON SUBSCRIPTRANGE SNAP BEGIN; PUT DATA
(I,KS,J,K,TX,TY,TZ);                    EXIT;
/*
READ IN THE PEAKS, SORTED BY LAYER
OPEN FILE (RETAIN) INPUT;
ALLOCATE PEAKS, IS;
DO I = 1 TO #RTND BY 1;
READ FILE (RETAIN) INTO (PEAKR);
U(I) = RU;
V(I) = RV;
W(I) = RW;
VALU(I) = VAL;
MEAN(I) = AVG;
END ILUP;
CLOSE FILE (RETAIN);
ION = '0'B;
NCNT = '0'B;
IA = IACR;
ID = IDWN;
IL = ILAY;
/*
TRANSFORM THE SYMMETRY ELEMENTS INTO MORE USEABLE FORM
DO I = 1 TO #SYMM BY 1;
IS(I) = 0;
IF (PX(I) = -1) THEN IS(I) = IS(I) + 1;
IF (PY(I) = -1) THEN IS(I) = IS(I) + 2;
IF (PZ(I) = -1) THEN IS(I) = IS(I) + 4;
IF (QX(I) = 1) THEN QX(I) = IACR / 2;
IF (QY(I) = 1) THEN QY(I) = IDWN / 2;
IF (QZ(I) = 1) THEN QZ(I) = ILAY / 2;
KS = IS(I);
IF (KS = 7) THEN DO;
XQ = QX(I);
YQ = QY(I);
ZQ = QZ(I);
ION(KS) = '1'B;
END SLUP;
PUT EDIT (#RTND,' PEAKS WERE RETAINED') (SKIP(2),F(5),A);
IF (DBG) THEN PUT EDIT('ION = ',ION) (SKIP,A,7 (B(1),X(1)));
ELSE;

```

```

-P2-1020
*/ -P2-1030
-P2-1040
-P2-1050
-P2-1060
-P2-1070
-P2-1080
-P2-1090
-P2-1100
END; -P2-1110
-P2-1120
*/ -P2-1130
-P2-1140
-P2-1150
-P2-1160
-P2-1170
-P2-1180
-P2-1190
-P2-1200
-P2-1210
-P2-1220
-P2-1230
-P2-1240
-P2-1250
-P2-1260
-P2-1270
-P2-1280
-P2-1290
-P2-1300
-P2-1310
-P2-1320
*/ -P2-1330
-P2-1340
-P2-1350
ELSE; -P2-1360
ELSE; -P2-1370
ELSE; -P2-1380
ELSE; -P2-1390
ELSE; -P2-1400
ELSE; -P2-1410
-P2-1420
-P2-1430
-P2-1440
-P2-1450
ELSE; -P2-1460
-P2-1470
-P2-1480
-P2-1490
-P2-1500
-P2-1510

```

```

/*
ALLOC:
AL(1):
AL(2):
AL(3):
AL(4):
AL(5):
AL(6):
AL(7):
NDA:
/*
OUTER:
INNER:
/*
IF (DBG) THEN PUT PAGE;
ELSE;
ALLOCATE ARRAYS FOR MIRRORS, GLIDES, TWO-FOLDS, AND SCREWS */
DO I = 1 TO 7;
IF (ION(I)) THEN GO TO AL(I);
ALLOCATE XLINE#;
XLINE# = 0.000;
NCNT = 1.0;
GO TO NDA;
ALLOCATE YLINE#;
YLINE# = 0.000;
NCNT = 1.0;
GO TO NDA;
ALLOCATE XYLAY#;
XYLAY# = 0.000;
NCNT = 1.0;
GO TO NDA;
ALLOCATE ZLINE#;
ZLINE# = 0.000;
NCNT = 1.0;
GO TO NDA;
ALLOCATE ZXLAY#;
ZXLAY# = 0.000;
NCNT = 1.0;
GO TO NDA;
ALLOCATE YZLAY#;
YZLAY# = 0.000;
NCNT = 1.0;
GO TO NDA;
LAY# = 0.0;
END ALLOC;
SGNL = ION(7);
SEARCH THROUGH ALL PEAKS
DO J = 1 TO #RTND BY 1;
JU = U(J);
JV = V(J);
JW = W(J);
DO I = J TO #RTND BY 1;
IU = U(I);
IV = V(I);
IW = W(I);
MEANJ = MEAN(J);
MEANIJ = FLOAT(MEANJ+MEAN(I))/TH;
I2 = J2 * MEANIJ;
I4 = J4 * MEANIJ;
I5 = J5 * MEANIJ;
I6 = J6 * MEANIJ;
COMPUTE THE SUM (P) AND THE DIFFERENCE (M) BETWEEN PEAKS
JU, JV, JW AND IU, IV, IW ALLOWING ONE GRID POINT POSITIVE (P)
AND NEGATIVE (M) ERROR
*/
1520
--P2-1530
--P2-1540
--P2-1550
--P2-1560
--P2-1570
--P2-1580
--P2-1590
--P2-1600
--P2-1610
--P2-1620
--P2-1630
--P2-1640
--P2-1650
--P2-1660
--P2-1670
--P2-1680
--P2-1690
--P2-1700
--P2-1710
--P2-1720
--P2-1730
--P2-1740
--P2-1750
--P2-1760
--P2-1770
--P2-1780
--P2-1790
--P2-1800
--P2-1810
--P2-1820
--P2-1830
--P2-1840
--P2-1850
--P2-1860
--P2-1870
--P2-1880
--P2-1890
--P2-1900
--P2-1910
--P2-1920
--P2-1930
--P2-1940
--P2-1950
--P2-1960
--P2-1970
--P2-1980
--P2-1990
--P2-2000
--P2-2010

```



```

JPIU = JU + IU;
JPIV = JV + IV;
JPIW = JW + IW;
JMIU = MOD (JU - IU + I4A, IACR);
JMIV = MOD (JV - IV + I4D, IDWN);
JMIW = MOD (JW - IW + I4L, ILAY);
JMIUP = MOD (JMIU + 1 + I4A, IACR);
JMIUM = MOD (JMIU - 1 + I4A, IACR);
JMIVP = MOD (JMIV + 1 + I4D, IDWN);
JMIVM = MOD (JMIV - 1 + I4D, IDWN);
JMIWP = MOD (JMIW + 1 + I4L, ILAY);
JMIWM = MOD (JMIW - 1 + I4L, ILAY);
/*
LOOP THROUGH ALL SYMMETRY ELEMENTS
SYML: DO K = 1 TO #SYMM BY 1;
      KS = IS (K);
      GO TO SYM(KS);
/*
MIRROR OR GLIDE PLANE PERPENDICULAR TO X; DETERMINE TX
NOTE P2(1) ABOVE THAT V2-V1 = QY+/-1 AND W2-W1 = QZ+/-1
BEFORE U2+U1 = QX+2TX HOLDS.
SYM(1): IF ((JMIVP = QY(K)) & (JMIV = QY(K)) & (JMIVM = QY(K)))
        THEN GO TO NDSY;
        ELSE;
        IF ((JMIWP = QZ(K)) & (JMIW = QZ(K)) & (JMIWM = QZ(K)))
        THEN GO TO NDSY;
        ELSE;
        TX = MOD (((JPIU - QX(K)) / 2) + I4A, IACR);
        XLINE#(TX) = XLINE#(TX) + I1;
        TX = MOD (TX + 1, IACR);
        XLINE#(TX) = XLINE#(TX) + I3;
        TX = MOD (TX - 2 + IACR, IACR);
        XLINE#(TX) = XLINE#(TX) + I3;
        GO TO NDSY;
/*
MIRROR OR GLIDE PLANE PERPENDICULAR TO Y; DETERMINE TY
NOTE P2(2) ABOVE THAT U2-U1 = QX+/-1 AND W2-W1 = QZ+/-1
BEFORE V2+V1 = GY+2TY HOLDS.
SYM(2): IF ((JMIUP = QX(K)) & (JMIU = QX(K)) & (JMIUM = QX(K)))
        THEN GO TO NDSY;
        ELSE;
        IF ((JMIWP = QZ(K)) & (JMIW = QZ(K)) & (JMIWM = QZ(K)))
        THEN GO TO NDSY;
        ELSE;
        TY = MOD (((JPIV - QY(K)) / 2) + I4D, IDWN);
        YLINE#(TY) = YLINE#(TY) + I1;
        TY = MOD (TY + 1, IDWN);
        YLINE#(TY) = YLINE#(TY) + I3;
        TY = MOD (TY - 2 + IDWN, IDWN);
        YLINE#(TY) = YLINE#(TY) + I3;
        GO TO NDSY;

```

```

-P2-2020
-P2-2030
-P2-2040
-P2-2050
-P2-2060
-P2-2070
-P2-2080
-P2-2090
-P2-2100
-P2-2110
-P2-2120
-P2-2130
-P2-2140
-P2-2150
*/ -P2-2160
-P2-2170
-P2-2180
-P2-2190
-P2-2200
-P2-2210
-P2-2220
-P2-2230
*/ -P2-2240
-P2-2250
-P2-2260
-P2-2270
-P2-2280
-P2-2290
-P2-2300
-P2-2310
-P2-2320
-P2-2330
-P2-2340
-P2-2350
-P2-2360
-P2-2370
-P2-2380
-P2-2390
*/ -P2-2400
-P2-2410
-P2-2420
-P2-2430
-P2-2440
-P2-2450
-P2-2460
-P2-2470
-P2-2480
-P2-2490
-P2-2500
-P2-2510

```

```

/*
TWO-FOLD OR TWO-FOLD SCREW AXIS IN Z; DETERMINE TX & TY
NOTE P2(3) ABOVE THAT W2-W1 = QZ+/-1 BEFORE U2+U1 = QX+2TX
AND V2+V1 = QY+2TY HOLDS.
SYM(3): IF ((JMIWP ^= QZ(K)) & (JMIW ^= QZ(K)) & (JMIWM ^= QZ(K)))
/*
ELSE;
TX = MOD (((JPIU - QX(K)) / 2) + I4A, IACR);
TY = MOD (((JPIV - QY(K)) / 2) + I4D, IDWN);
XYLAY#(TX, TY) = XYLAY#(TX, TY) + I2;
TXP = MOD (TX + 1, IACR);
TXM = MOD (TX - 1, IACR);
TYM = MOD (TY - 1, IDWN);
XYLAY#(TX, TY) = XYLAY#(TX, TY) + I4;
XYLAY#(TXP, TY) = XYLAY#(TXP, TY) + I4;
XYLAY#(TXM, TY) = XYLAY#(TXM, TY) + I4;
XYLAY#(TXM, TY) = XYLAY#(TXM, TY) + I6;
XYLAY#(TXM, TYM) = XYLAY#(TXM, TYM) + I6;
XYLAY#(TXP, TYM) = XYLAY#(TXP, TYM) + I6;
XYLAY#(TXP, TY) = XYLAY#(TXP, TY) + I6;
GO TC NDSY;
/*
MIRRCR OR GLIDE PLANE PERPENDICULAR TO Z; DETERMINE TZ
NOTE P2(4) ABOVE THAT U2-U1 = QX+/-1 AND V2-V1 = QY+/-1
BEFORE W2+W1 = QZ+2TZ HOLDS
SYM(4): IF ((JMIUP ^= QX(K)) & (JMIU ^= QX(K)) & (JMIUM ^= QX(K)))
/*
ELSE;
IF ((JMIVP ^= QY(K)) & (JMIV ^= QY(K)) & (JMIVM ^= QY(K)))
ELSE;
TZ = MOD (((JPIW - QZ(K)) / 2) + I4L, ILAY);
ZLINE#(TZ) = ZLINE#(TZ) + I1;
TZ = MOD (TZ + 1, ILAY);
ZLINE#(TZ) = ZLINE#(TZ) + I3;
TZ = MOD (TZ - 2, ILAY);
ZLINE#(TZ) = ZLINE#(TZ) + I3;
GO TC NDSY;
/*
TWO-FOLD OR TWO-FOLD SCREW AXIS IN Y; DETERMINE TX & TZ
NOTE P2(5) ABOVE THAT V2-V1 = QY+/-1 BEFORE U2+U1 = QX+2TX
AND W2+W1 = QZ+2TZ HOLDS.
SYM(5): IF ((JMIVP ^= QY(K)) & (JMIV ^= QY(K)) & (JMIVM ^= QY(K)))
/*
ELSE;
TX = MOD (((JPIU - QX(K)) / 2) + I4A, IACR);
TZ = MOD (((JPIW - QZ(K)) / 2) + I4L, ILAY);
ZXLAY#(TZ, TX) = ZXLAY#(TZ, TX) + I2;
TZP = MOD (TZ + 1, ILAY);

```

--P2-2520

--P2-2530

--P2-2540

--P2-2550

--P2-2560

--P2-2570

--P2-2580

--P2-2590

--P2-2600

--P2-2610

--P2-2620

--P2-2630

--P2-2640

--P2-2650

--P2-2660

--P2-2670

--P2-2680

--P2-2690

--P2-2700

--P2-2710

--P2-2720

--P2-2730

--P2-2740

--P2-2750

--P2-2760

--P2-2770

--P2-2780

--P2-2790

--P2-2800

--P2-2810

--P2-2820

--P2-2830

--P2-2840

--P2-2850

--P2-2860

--P2-2870

--P2-2880

--P2-2890

--P2-2900

--P2-2910

--P2-2920

--P2-2930

--P2-2940

--P2-2950

--P2-2960

--P2-2970

--P2-2980

--P2-2990

--P2-3000

--P2-3010

```

- P2-3020
- P2-3030
- P2-3040
- P2-3050
- P2-3060
- P2-3070
- P2-3080
- P2-3090
- P2-3100
- P2-3110
- P2-3120
- P2-3130
- P2-3140
- P2-3150
- P2-3160
- P2-3170
- P2-3180
- P2-3190
- P2-3200
- P2-3210
- P2-3220
- P2-3230
- P2-3240
- P2-3250
- P2-3260
- P2-3270
- P2-3280
- P2-3290
- P2-3300
- P2-3310
- P2-3320
- P2-3330
- P2-3340
- P2-3350
- P2-3360
- P2-3370
- P2-3380
- P2-3390
- P2-3400
- P2-3420
- P2-3430
- P2-3440
- P2-3450
- P2-3460
- P2-3470
- P2-3480
- P2-3490
- P2-3500
- P2-3510

TXP = MOD (TX + 1, IACR);
TXM = MOD (TX - 1, IACR);
TXM = MOD (TX - 1, IACR);
ZXLAY#(TXP) = ZXLAY#(TXP) + I4;
ZXLAY#(TXM) = ZXLAY#(TXM) + I4;
ZXLAY#(TZP, TX) = ZXLAY#(TZP, TX) + I4;
ZXLAY#(TZM, TX) = ZXLAY#(TZM, TX) + I4;
ZXLAY#(TZM, TXP) = ZXLAY#(TZM, TXP) + I6;
ZXLAY#(TZM, TXM) = ZXLAY#(TZM, TXM) + I6;
ZXLAY#(TZP, TXM) = ZXLAY#(TZP, TXM) + I6;
ZXLAY#(TZP, TXP) = ZXLAY#(TZP, TXP) + I6;
GO TC NDSY;

/*
TWO-FOLD OR TWO-FOLD SCREW AXIS IN X; DETERMINE TY & TZ
NOTE P2(6) ABOVE THAT U2-U1 = QX+/-1 BEFORE V2+V1 = QY+2TY
AND W2+W1 = QZ+2TZ
SYM(6): IF ((JMIUP - QX(K)) & (JMIU - QX(K)) & (JMIUM - QX(K)))
        THEN GO TO NDSY;
        ELSE;
        TZ = MOD (((JPIW - QZ(K)) / 2) + I4L, ILAY);
        TY = MOD (((JPIV - QY(K)) / 2) + I4D, IDWN);
        YZLAY#(TY, TZ) = YZLAY#(TY, TZ) + I2;
        TYP = MOD (TY + 1, IDWN);
        TYM = MOD (TY - 1, IDWN);
        TZM = MOD (TZ - 1, IDWN);
        YZLAY#(TY, TZP) = YZLAY#(TY, TZP) + I4;
        YZLAY#(TY, TZM) = YZLAY#(TY, TZM) + I4;
        YZLAY#(TYM, TZ) = YZLAY#(TYM, TZ) + I4;
        YZLAY#(TYM, TZP) = YZLAY#(TYM, TZP) + I6;
        YZLAY#(TYM, TZM) = YZLAY#(TYM, TZM) + I6;
        YZLAY#(TYP, TZP) = YZLAY#(TYP, TZP) + I6;
        GO TC NDSY;

/*
CENTER OF INVERSION; DETERMINE TX, TY, & TZ
SYM(7): TZ = MOD ((JPIW - ZQ) / 2) + I4L, ILAY);
/*
DETERMINE THE LAYERS WITH TX.TY.TZ
DO IZ = -1 TC 1 BY 1;
JZ = MOD (IZ + IZ + ILAY, ILAY);
LAY#(JZ) = I8;
END OUTPUT;
END SYML;
END INNER;
IF (CBG) THEN PUT EDIT (' PEAK# =', J) (A, F(4));
END CUTER;

NDSY:
ELSE;
*/

```

RETURN;
END PART2;

-P2-3520
-P2-3530

```
* PROCESS('ATR,XREF,NOSTMT,OPT=02');
/* OUTPUT ALL VALUES OF TX.TY.TZ WITH FREQUENCY > 5 TO BE SORTED */
PART3: PROCEDURE (IACR,IDWN,ILAY,#RTND);
/*
    IN PART2, ALL OF THE POSSIBLE VALUES OF TZ WERE FLAGGED AS
    TO WHETHER OR NOT THEY OCCURRED. IN THIS SUBROUTINE, A LAYER OF
    TX.TY IS FILLED FOR EACH VALUE OF TZ, WITH THE FREQUENCY OF
    OCCURRENCE OF EACH VALUE OF TX.TY.TZ. AFTER THE LAYER HAS BEEN
    CREATED, ALL OF THE TX.TY.TZ TRIPLES WITH FREQUENCY > 5 ARE OUTPUT
    */
    DECLARE LAYER (0:IACR,0:IDWN)      FLOAT BIN CTL;
    DECLARE LAY#(0:ILAY)              EXTERNAL BIT(1) CTL;
    DECLARE (IACR,IDWN,ILAY,#RTND)    FIXED BINARY (15);
    DECLARE SORTIN                    FILE RECORD SEQUENTIAL;
    DECLARE (DBG,DNV)                EXTERNAL BIT (1);
    DECLARE 1 PEAKS (#RTND)           CONTROLLED EXTERNAL,
    2 (U,V,W,VALU,MEAN)              FIXED BINARY (15);
    DECLARE 1 SXYZ,
    2 (SX,SY,SZ,SK)                  FIXED BINARY (15),
    2 (VAL,AVG,FREQ)                 FLCAT BINARY;
    DECLARE (O2,O3,O4,O5,M1,M2,M3,TH) FLOAT BINARY;
    DECLARE (XQ,YQ,ZQ)              EXTERNAL FIXED BIN;
    DECLARE #INV                    FIXED BIN;
    #INV = 0;                       TH = 50.000;
    O2 = 2.00;
    O3 = 3.00;
    O4 = 4.00;
    O5 = 5.00;
    X5 = O5 * 5.0000;
    VAL,AVG = 0.0000;
    SK = 7;
    I4A = IACR * 4;
    I4D = IDWN * 4;
    I4L = ILAY * 4;
    ON ERROR SNAP EXIT;
    IF (DBG) THEN PUT EDIT ('XQ = ',XQ,'YQ = ',YQ,'ZQ = ',ZQ)
    (SKIP(4),3 (A,F(5),X(2))); ELSE;
    IF (DBG) THEN PUT EDIT ('LAY# = ',LAY#)
    (SKIP(2),A,(ILAY+1) (X(2),B(1))); ELSE;
    IF (DNV) THEN DO;
    PUT EDIT ('THE TX, TY, TZ PAIRS THAT HAVE MORE THAN 5',
    ' TX TY TZ SY VALU MEAN FREQ',
    ' TX TY TZ SY VALU MEAN FREQ',
    ' TX TY TZ SY VALU MEAN FREQ',
    -P3-0010
    -P3-0020
    -P3-0030
    -P3-0040
    -P3-0050
    -P3-0060
    -P3-0070
    -P3-0080
    -P3-0090
    -P3-0100
    -P3-0110
    -P3-0120
    -P3-0130
    -P3-0140
    -P3-0150
    -P3-0160
    -P3-0170
    -P3-0180
    -P3-0190
    -P3-0200
    -P3-0210
    -P3-0220
    -P3-0230
    -P3-0240
    -P3-0250
    -P3-0260
    -P3-0270
    -P3-0280
    -P3-0290
    -P3-0300
    -P3-0310
    -P3-0320
    -P3-0330
    -P3-0340
    -P3-0350
    -P3-0360
    -P3-0370
    -P3-0380
    -P3-0390
    -P3-0400
    -P3-0410
    -P3-0420
    -P3-0430
    -P3-0440
```

```

          ' TX TY TZ SY VALU MEAN FREQ')
          (PAGE,A,SKIP,A,A,A,A); PUT SKIP;
OPEN FILE (SORTIN) OUTPUT;
ALLOCATE LAYER;
/*
LOOP THROUGH THE LAYERS, ONE AT A TIME
IF (~LAY#( LAY)) THEN GO TO NDLAY;
LAYLUP: DO LAY = 0 TC ILAY BY 1;
LAYER = 0.000;
/*
OUTER LOOP THROUGH ALL THE PEAKS
CUTER: DO J = 1 TO #RTND BY 1; MEANJ = MEAN(J);
K = J + 1;
IF (K > #RTND) THEN GO TO NDOTR;
JU = U(J);
JV = V(J);
JW = W(J);
/*
INNER LOOP THROUGH THE REMAINDER OF THE PEAKS
INNER: DO I = K TO #RTND BY 1; MEANIJ=FLOAT(MEANJ+MEAN(I))/TH;
JPIW = MOD (((JW + W(I) - ZQ) / 2) + I4L, ILAY);
JPIWP = MOD (JPIW + 1, ILAY);
JPIWM = MOD (JPIW - 1 + ILAY, ILAY);
IF (JPIW = LAY) THEN GO TO RTON;
IF ((JPIWP = LAY)|(JPIWM = LAY)) THEN GO TO ZOFF1;
ELSE GO TO NDINR;
/*
THE VALUE OF ILAY = TZ
RTON: M1 = 05 * MEANIJ;
M2 = 04 * MEANIJ;
M3 = 03 * MEANIJ;
GO TC OK;
/*
THE VALUE OF ILAY = TZ+1 OR TZ-1
ZOFF1: M1 = 04 * MEANIJ;
M2 = 03 * MEANIJ;
M3 = 02 * MEANIJ;
/*
SET UP THE VALUES OF TX AND TY OFF ONE GRID POINT
OK: JPIU = MOD (((JU + U(I) - XQ) / 2) + I4A, IACR);
JPIV = MOD (((JV + V(I) - YQ) / 2) + I4D, IDWN);
JPIUP = MOD (JPIU + 1, IACR);
JPIVP = MOD (JPIV + 1, IDWN);
JPIUM = MOD (JPIU - 1 + IACR, IACR);

```

```

END; ELSE; -P3-0450
-P3-0460
-P3-0470
-P3-0480
-P3-0490
-P3-0500
ELSE; -P3-0510
*/ -P3-0520
-P3-0530
-P3-0540
-P3-0550
*/ -P3-0560
-P3-0570
-P3-0580
-P3-0590
ELSE; -P3-0600
-P3-0610
-P3-0620
-P3-0630
-P3-0640
*/ -P3-0650
-P3-0660
-P3-0670
-P3-0680
-P3-0690
-P3-0700
ELSE; -P3-0710
-P3-0720
-P3-0730
-P3-0740
*/ -P3-0750
-P3-0760
-P3-0770
-P3-0780
-P3-0790
-P3-0800
-P3-0810
-P3-0820
*/ -P3-0830
-P3-0840
-P3-0850
-P3-0860
-P3-0870
-P3-0880
*/ -P3-0890
-P3-0900
-P3-0910
-P3-0920
-P3-0930
-P3-0940

```

```

/*          JPIVM = MOD (JPIV - 1 + IDWN, IDWN);          -P3-0950
/*          FILL THE ARRAY WITH THE FREQUENCIES          -P3-0960
/*          */ -P3-0970
FILL:      LAYER (JPIU ,JPIV )  =  LAYER (JPIU ,JPIV ) + M1;  -P3-0980
          LAYER (JPIU ,JPIVP)  =  LAYER (JPIU ,JPIVP) + M2;  -P3-0990
          LAYER (JPIU ,JPIVM)  =  LAYER (JPIU ,JPIVM) + M2;  -P3-1000
          LAYER (JPIUP,JPIV )  =  LAYER (JPIUP,JPIV ) + M2;  -P3-1010
          LAYER (JPIUP,JPIVP)  =  LAYER (JPIUP,JPIVP) + M3;  -P3-1020
          LAYER (JPIUP,JPIVM)  =  LAYER (JPIUP,JPIVM) + M3;  -P3-1030
          LAYER (JPIUM,JPIV )  =  LAYER (JPIUM,JPIV ) + M2;  -P3-1040
          LAYER (JPIUM,JPIVP)  =  LAYER (JPIUM,JPIVP) + M3;  -P3-1050
          LAYER (JPIUM,JPIVM)  =  LAYER (JPIUM,JPIVM) + M3;  -P3-1060
NDINR:    END INNER;          -P3-1070
NDOTR:    END OUTER;        -P3-1080
/*          WRITE OUT THE TX.TY.TZ TRIPLES FROM THE LAYER  -P3-1090
/*          */ -P3-1100
          SZ = LAY;          -P3-1110
SYLP:    DO SY = 0 TO IDWN BY 1;  -P3-1120
SXLP:    DO SX = 0 TO IACR BY 1;  -P3-1130
          FREQ = LAYER (SX,SY);  -P3-1140
          IF (FREQ > X5) THEN GO TO OUTP;      ELSE GO TO NDSX;  -P3-1150
OUTP:    WRITE FILE (SORTIN) FROM (SXYZ);  -P3-1160
          #INV = #INV + 1;  -P3-1170
          IF (CNV) THEN PUT EDIT (SXYZ) (4 F(3),3 F(7));  ELSE;  -P3-1180
NDSX:    END SXLP;          -P3-1190
          END SYLP;          -P3-1200
NDLAY:   END LAYLUP;        -P3-1210
          FREE LAYER, LAY#, PEAKS;  -P3-1220
          PUT EDIT('THERE ARE',#INV,'TX.TY.TZ TRIPLES FROM INVERSIONS.') -P3-1230
          (SKIP(2),A,F(10),X(1),A);  -P3-1240
          PUT EDIT ('***** ALL INVERSIONS HAVE BEEN OUTPUT *****') -P3-1250
          (SKIP(2),A);  -P3-1260
          RETURN;  -P3-1270
          END PART3;  -P3-1280
          -P3-1290
          -P3-1300

* PROCESS('ATR,XREF,NOSTMT,OPT=02');  -P4-0010
/*  OUTPUT TX, TY, TZ, TX.TY, TY.TZ, TZ.TX WITH FREQUENCY > 10  */ -P4-0020
PART4:  PROCEDURE (IACR, IDWN, ILAY);  -P4-0030
/*          -P4-0040
          IN PART2 THE TX, TY, TZ, TX.TY, TY.TZ, TX.TZ GROUP(S) ARE PRODUCED -P4-0050
          FROM THE NON-INVERSION SYMMETRY ELEMENTS. THESE VALUES OF  -P4-0060
          THE TRANSLATIONS ARE STORED IN THE EXTERNAL ARRAYS XLINE#,  -P4-0070
          YLINE#, ZLINE#, XYLAY#, YZLAY#, ZXLAY#. THESE VALUES ARE  -P4-0080
          WRITTEN OUT ON THE FILE "SORTIN", WITH THE UNDETERMINED VALUES -P4-0090
          SET EQUAL TO -1.  -P4-0100

```

```

DECLARE (IACR,IA,IDWN,ID,ILAY,IL) FIXED BINARY (15);          */ -P4-0110
DECLARE ION(7) BIT (1) EXTERNAL;                               -P4-0120
DECLARE SORTIN FILE RECORD SEQUENTIAL;                         -P4-0130
DECLARE SLB(6) LABEL;                                          -P4-0140
DECLARE (XLINE#(0:IACR), YLINE#(0:IDWN), ZLINE#(0:ILAY),      -P4-0150
        XYLAY#(0:IA,0:ID), YZLAY#(0:ID,0:IL), ZXLAY#(0:IL,0:IA)) -P4-0160
        EXTERNAL CONTROLLED FLOAT BINARY;                       -P4-0170
                                                                -P4-0180
DECLARE 1 SXYZ,                                                -P4-0190
        2 (SX, SY, SZ, SK) FIXED BINARY (15),                 -P4-0200
        2 (VALU,MEAN,FREQ) FLOAT BINARY;                       -P4-0210
                                                                -P4-0220
DECLARE TEN FLOAT BINARY;                                      -P4-0230
DECLARE DBG EXTERNAL BIT (1);                                  -P4-0240
TEN = 10.000;                                                 -P4-0250
IA = IACR;                                                     -P4-0260
ID = IDWN;                                                      -P4-0270
IL = ILAY;                                                       -P4-0280
VALU, MEAN = 1.000;                                           -P4-0290
ON SUBSCRIPTRANGE SNAP BEGIN; PUT DATA                        -P4-0300
(SK,SX,SY,SZ);                                               EXIT;                               END; -P4-0310
IF (DBG) THEN DO;                                             -P4-0320
PUT EDIT ('PEAKS FROM MIRRORS, GLIDES, TWO-FOLDS, & SCREWS', -P4-0330
        ' SX SY SZ TY VALUE MEAN FREQ',
        ' SX SY SZ TY VALUE MEAN FREQ',
        ' SX SY SZ TY VALUE MEAN FREQ',
        ' SX SY SZ TY VALUE MEAN FREQ');
                                                                -P4-0340
                                                                -P4-0350
                                                                -P4-0360
        (PAGE,A,SKIP,A,A,A,A);
                                                                -P4-0370
PUT SKIP;                                                     ELSE; -P4-0380
                                                                -P4-0390
/*
GO THROUGH ALL OF THE SIX NON-INVERSION SYMMETRY TYPES      */ -P4-0400
                                                                -P4-0410
STYP: DO SK = 1 TO 6 BY 1;                                     -P4-0420
IF (ION(SK)) THEN GO TO SLB(SK);                               ELSE GO TO NDS; -P4-0430
                                                                -P4-0440
/*
OUTPUT ALL TX WITH # > 10 FOR A PLANE NORMAL TO X          */ -P4-0450
                                                                -P4-0460
SLB(1): SY, SZ = -1;                                          -P4-0470
XLUP: DO SX = 0 TO IACR BY 1;                                  -P4-0480
IF (XLINE#(SX) < TEN) THEN GO TO NDX;                          ELSE; -P4-0490
FREQ = XLINE#(SX);                                           -P4-0500
IF (DBG) THEN PUT EDIT (SXYZ) (4 F(3),3 F(7,0));             ELSE; -P4-0510
WRITE FILE (SORTIN) FROM (SXYZ);                               -P4-0520
NDX: END XLUP;                                                -P4-0530
FREE XLINE#;                                                  -P4-0540
GO TO NDS;                                                    -P4-0550
                                                                -P4-0560
/*
OUTPUT ALL TY WITH # > 10 FOR A PLANE NORMAL TO Y          */ -P4-0570
                                                                -P4-0580
SLB(2): SX, SZ = -1;                                          -P4-0590
YLUP: DO SY = 0 TO IDWN BY 1;                                  -P4-0600

```

```

IF (YLINE#(SY) < TEN) THEN GO TO NDY;
FREQ = YLINE#(SY);
IF (DBG) THEN PUT EDIT (SXYZ) (4 F(3),3 F(7,0));
WRITE FILE (SORTIN) FROM (SXYZ);
NDY:
END YLUP;
FREE YLINE#;
GO TC NDS;

/*
OUTPUT ALL TX.TY WITH # > 10 FOR AN AXIS IN Z
*/
SLB(3): SZ = -1;
XLXY: DO SX = 0 TO IACR BY 1;
YLXY: DO SY = 0 TO IDWN BY 1;
IF (XYLAY#(SX,SY) < TEN) THEN GO TO NDXY;
FREQ = XYLAY#(SX,SY);
IF (DBG) THEN PUT EDIT (SXYZ) (4 F(3),3 F(7,0));
WRITE FILE (SORTIN) FROM (SXYZ);
NDXY:
END YLXY;
END XLXY;
FREE XYLAY#;
GO TC NDS;

/*
OUTPUT ALL TZ WITH # > 10 FOR A PLANE NORMAL TO Z
*/
SLB(4): SX, SY = -1;
ZLUP: DO SZ = 0 TO ILAY BY 1;
IF (ZLINE#(SZ) < TEN) THEN GO TO NDZ;
FREQ = ZLINE#(SZ);
IF (DBG) THEN PUT EDIT (SXYZ) (4 F(3),3 F(7,0));
WRITE FILE (SORTIN) FROM (SXYZ);
NDZ:
END ZLUP;
FREE ZLINE#;
GO TC NDS;

/*
OUTPUT ALL TZ.TX WITH # > 10 FOR AN AXIS IN Y
*/
SLB(5): SY = -1;
ZLZX: DO SZ = 0 TO ILAY BY 1;
XLZX: DO SX = 0 TO IACR BY 1;
IF (ZXLAY#(SZ,SX) < TEN) THEN GO TO NDZX;
FREQ = ZXLAY#(SZ,SX);
IF (DBG) THEN PUT EDIT (SXYZ) (4 F(3),3 F(7,0));
WRITE FILE (SORTIN) FROM (SXYZ);
NDZX:
END XLZX;
END ZLZX;
FREE ZXLAY#;
GO TO NDS;

/*
OUTPUT ALL TY.TZ WITH # > 10 FOR AN AXIS IN X
*/
ELSE; -P4-0610
ELSE; -P4-0620
ELSE; -P4-0630
ELSE; -P4-0640
ELSE; -P4-0650
ELSE; -P4-0660
ELSE; -P4-0670
ELSE; -P4-0680
ELSE; -P4-0690
*/ -P4-0700
ELSE; -P4-0710
ELSE; -P4-0720
ELSE; -P4-0730
ELSE; -P4-0740
ELSE; -P4-0750
ELSE; -P4-0760
ELSE; -P4-0770
ELSE; -P4-0780
ELSE; -P4-0790
ELSE; -P4-0800
ELSE; -P4-0810
ELSE; -P4-0820
ELSE; -P4-0830
*/ -P4-0840
ELSE; -P4-0850
ELSE; -P4-0860
ELSE; -P4-0870
ELSE; -P4-0880
ELSE; -P4-0890
ELSE; -P4-0900
ELSE; -P4-0910
ELSE; -P4-0920
ELSE; -P4-0930
ELSE; -P4-0940
ELSE; -P4-0950
*/ -P4-0960
ELSE; -P4-0970
ELSE; -P4-0980
ELSE; -P4-0990
ELSE; -P4-1000
ELSE; -P4-1010
ELSE; -P4-1020
ELSE; -P4-1030
ELSE; -P4-1040
ELSE; -P4-1050
ELSE; -P4-1060
ELSE; -P4-1070
ELSE; -P4-1080
ELSE; -P4-1090
*/ -P4-1100

```



```

SLB(6):  SX = -1;
YLYZ:   DO SY = 0 TO IDWN BY 1;
ZLYZ:   DO SZ = 0 TO ILAY BY 1;
        IF (YZLAY#(SY,SZ) < TEN) THEN GO TO NDYZ; ELSE;
        FREQ = YZLAY#(SY,SZ); ELSE;
        IF (DBG) THEN PUT EDIT (SXYZ) (4 F(3),3 F(7,0)); ELSE;
        WRITE FILE (SORTIN) FROM (SXYZ);
NDYZ:   END ZLYZ;
        END YLYZ;
        FREE YZLAY#;
NDS:   END STYP;
        RETURN;
        END PART4;

```

```

-P4-1110
-P4-1120
-P4-1130
-P4-1140
-P4-1150
-P4-1160
-P4-1170
-P4-1180
-P4-1190
-P4-1200
-P4-1210
-P4-1220
-P4-1230

```

```

* PROCESS('ATR,XREF,NOSTMT,OPT=02');
/* MAP THE SYMMETRY ELEMENTS INTO EACH OTHER */
PART5: PROCEDURE (IACR, IDWN, ILAY);
/*
BEFORE THIS PART, THE VALUE OF TX, TY, TZ, TX.TY, TX.TZ, TY.TZ. &
TX.TY.TZ WRITTEN OUT BY PART3 AND PART4, WERE SORTED BY
DECREASING FREQUENCY (SO THAT THE MOST FREQUENT ARE FIRST) &
BY DECREASING SYMMETRY (SO THAT THE INVERSIONS ARE FIRST).
A NUMBER OF EACH OF THESE, PROPORTIONAL TO THE SIZE OF THE
MAP AND TO THE TOTAL NUMBER OF EACH SYMMETRY ELEMENT POSSIBLE,
IS NOW READ AND STORED. AT THIS POINT, THE SYMMETRY ELEMENTS
ARE MAPPED INTO EACH OTHER, AS SHOWN BELOW, WITH A LATITUDE
OF ONE GRID POINT ALLOWED IN EACH DIRECTION:

```

SYMMETRY ELEMENT	SYMMETRY ELEMENT MAPPED INTO
TX	TX.TY, TX.TZ, TX.TY.TZ
TY	TX.TY, TY.TZ, TX.TY.TZ
TZ	TX.TZ, TY.TZ, TX.TY.TZ
TX.TY	TY.TZ, TX.TZ, TX.TY.TZ
TX.TZ	TX.TY, TY.TZ, TX.TY.TZ
TY.TZ	TX.TY, TX.TZ, TX.TY.TZ

```

A RECORD IS KEPT AS EACH MAPPING IS DONE. ALSO, THE SUMS OF
THE FREQUENCIES ENCOUNTERED BY EACH MAPPING ARE COMPUTED AND
STORED.

```

```

DECLARE (IACR, IDWN, ILAY) FIXED BINARY (15);
DECLARE (IA8, ID8, IL8, #XYZ) FIXED BINARY (15) EXTERNAL;
DECLARE 1 TXYZ,
        2 (TX, TY, TZ, SK) FIXED BINARY (15),
        2 (VALU, MEAN, FRQ) FLOAT BINARY;
DECLARE SORTOUT FILE RECORD SEQUENTIAL;
DECLARE (IONI7), SGNL, NCNT) BIT (1) EXTERNAL;

```

```

-P5-0010
-P5-0020
-P5-0030
-P5-0040
-P5-0050
-P5-0060
-P5-0070
-P5-0080
-P5-0090
-P5-0100
-P5-0110
-P5-0120
-P5-0130
-P5-0140
-P5-0150
-P5-0160
-P5-0170
-P5-0180
-P5-0190
-P5-0200
-P5-0210
-P5-0220
-P5-0230
-P5-0240
-P5-0250
-P5-0260
-P5-0270
-P5-0280
-P5-0290
-P5-0300
-P5-0310
-P5-0320
-P5-0330

```

```

DECLARE 1 STORE (#XYZ)          CONTROLLED, (15),
2 (SX, SY, SZ, KS)             FLOAT BINARY; (15);
DECLARE 1 (CST(7), TST(7))     FIXED BINARY; (15);
2 (RX, RY, RZ, RS)             CONTROLLED EXTERNAL,
2 (BX, BY, BXY, BZ)           FIXED BINARY; (15);
2 OK                             BXYZ; BYZ);
DECLARE (FREQ1, P1, P2, P0)    FLOAT BINARY;
DECLARE CK(7)                   LABEL;
ON SUBSCRIPT RANGE SNAP BEGIN; EXTERNAL BIT (1);
(SK,I,J,KSI,IS,KSJ);          PUT DATA
                                EXIT;
                                END;
/*
P0:  RIGHT ON
P1:  OFF ONE GRID POINT IN ONE DIRECTION
P2:  OFF ONE GRID POINT IN EACH OF TWO DIRECTIONS
P1 = 0.8500;
P2 = 0.7000;
P0 = 1.0000;
/*
ALLOCATE ARRAY TO HOLD THE LARGEST TX, TY, TZ / SYMM TYPE
IA8 = IACR / 4;
ID8 = IDWN / 4;
IL8 = ILAY / 4;
TST(1) = ION(1) * IA8 * 2;
TST(2) = ION(2) * IA8 * 2;
TST(3) = ION(3) * IA8 * 2;
TST(4) = ION(4) * IA8 * 2;
TST(5) = ION(5) * IA8 * 2;
TST(6) = ION(6) * IA8 * 2;
TST(7) = ION(7) * IA8 * 2;
#XYZ = TST(1)+TST(2)+TST(3)+TST(4)+TST(5)+TST(6)+TST(7);
IF (IDBG) THEN PUT EDIT (TST(1),TST(2),TST(3),TST(4),TST(5),TST(6),TST(7),
(SKIP,A,7 B(1))); ELSE;
ALLOCATE STORE;
FREQ = 0.000;
CST = 0;
/*
READ IN THE HIGHEST VALUES OF TX, TY, TZ
ON ENDFILE (SORTOUT) GO TO FIND;
I = 0;
READ FILE (SORTOUT) INTO (TXYZ);
IF (CST(SK) >= TST(SK)) THEN GO TO RRD;
CST(SK) = CST(SK) + 1;
I = I + 1;
SX(I) = TX;
RRD:
ELSE;
P5-0340
P5-0350
P5-0360
P5-0370
P5-0380
P5-0390
P5-0400
P5-0410
P5-0420
P5-0430
P5-0440
P5-0450
P5-0460
P5-0470
P5-0480
P5-0490
P5-0500
P5-0510
P5-0520
P5-0530
P5-0540
P5-0550
P5-0560
P5-0570
P5-0580
P5-0590
P5-0600
P5-0610
P5-0620
P5-0630
P5-0640
P5-0650
P5-0660
P5-0670
P5-0680
P5-0690
P5-0700
P5-0710
P5-0720
P5-0730
P5-0740
P5-0750
P5-0760
P5-0770
P5-0780
P5-0790
P5-0800
P5-0810
P5-0820
P5-0830

```

```

SY(I) = TY; -P5-0840
SZ(I) = TZ; -P5-0850
KS(I) = SK; -P5-0860
FREQ(I) = FREQ(I) + FRQ; -P5-0870
IF (I < #XYZ) THEN GO TO RRD; ELSE; -P5-0880
/* -P5-0890
MERGE THE LOWER SYMMETRY ELEMENTS INTO THE HIGHER */ -P5-0900
FIND: CLOSE FILE (SORTOUT); -P5-0910
ALLOCATE RESULT; -P5-0920
BX, BY, BXY, BZ, BXZ, BYZ = '0'B; -P5-0930
RX = SX; -P5-0940
RY = SY; -P5-0950
RZ = SZ; -P5-0960
RS = KS; -P5-0970
OK = 0.000; -P5-0980
IF (DBG) THEN DO; -P5-0990
PUT EDIT ('SAVED TX, TY, TZ -- BEFORE MAPPING')(PAGE, A); -P5-1000
PUT EDIT (' TX TY TZ SY FREQ TX TY TZ SY FREQ', -P5-1010
' TX TY TZ SY FREQ TX TY TZ SY FREQ', -P5-1020
' TX TY TZ SY FREQ TX TY TZ SY FREQ'); -P5-1030
PUT EDIT ((SKIP(2),A,A,A); PUT SKIP(2); -P5-1040
PUT EDIT ((STORE (I) DO I = 1 TO #XYZ)) (4 F(3),E(10,3,4)); -P5-1050
END; ELSE; -P5-1060
ILUP: DO I = 1 TO #XYZ BY 1; -P5-1070
IS = KS(I); -P5-1080
ISX = SX(I); -P5-1090
ISY = SY(I); -P5-1100
ISZ = SZ(I); -P5-1110
FREQI = FREQ(I); -P5-1120
JLUP: DO J = 1 TO #XYZ BY 1; -P5-1130
KSJ = KS(J); -P5-1140
GO TO CK(KSJ); -P5-1150
/* -P5-1160
MERGE MIRRORS AND GLIDES WITH SCREWS, TWO-FOLDS AND INVERSIONS -P5-1170
MERGE TX WITH TX.TY, TX.TZ, OR TX.TY.TZ -P5-1180
/* -P5-1190
CK(1): IF ((IS=1)|(IS=2)|(IS=4)|(IS=6)) THEN GO TO NDJ; ELSE; -P5-1200
IDX = ABS (ISX - SX(J)); -P5-1210
IF (IDX < 2) THEN BX(I),BX(J) = '1'B; ELSE; -P5-1220
CMPX: IF (IDX=0) THEN OK(I) = OK(I) + (FREQI * FREQ(J)); ELSE; -P5-1230
IF (IDX=1) THEN OK(I) = OK(I) + (P1 * FREQI * FREQ(J)); ELSE; -P5-1240
GO TO NDJ; -P5-1250
/* -P5-1260
MERGE TY WITH TX.TY, TY.TZ OR TX.TY.TZ -P5-1270
/* -P5-1280
CK(2): IF ((IS=1)|(IS=2)|(IS=4)|(IS=5)) THEN GO TO NDJ; ELSE; -P5-1290
IDY = ABS (ISY - SY(J)); -P5-1300
IF (IDY < 2) THEN BY(I),BY(J) = '1'B; ELSE; -P5-1310
CMPY: IF (IDY=0) THEN OK(I) = OK(I) + (FREQI * FREQ(J)); ELSE; -P5-1320
-P5-1330

```



```

IDY = ABS (ISY - SY(J));
IDZ = ABS (ISZ - SZ(J));
IF ((IDY<2) & (IDZ<2)) THEN BYZ(I),BYZ(J)='1'B; ELSE;
ID1 = IDY;
ID2 = IDZ;
IF (IS=3) THEN IF (IDY>1) THEN GO TO NDJ;
ELSE DO; BYZ(I) = '1'B;
IF (IS=5) THEN IF (IDZ>1) THEN GO TO NDJ;
ELSE DO; BYZ(I) = '1'B;
IF ((IS=7)&(IDY<2)&(IDZ<2)) THEN GO TO CMPXYZ;
ELSE GO TO NDJ;
CMPXYZ: IF (ID1=0) THEN IF (ID2=0) THEN P = P0;
ELSE P = P1;
ELSE IF (ID2=0) THEN P = P1;
ELSE P = P2;
CK(7): OK(J) = OK(J) + (P * FREQI * FREQ(J));
NDJ: END JLUP;
END ILUP;
OK = OK * ((1000.000 * FLOAT(#XYZ)) / SUM(OK));
IF (DBG) THEN DO;
PUT EDIT ('SAVED TX, TY, TZ --- AFTER MAPPING')(SKIP(3),A);
PUT EDIT (' TX TY TZ SY FREQ TX TY TZ SY FREQ',
' TX TY TZ SY FREQ TX TY TZ SY FREQ',
' TX TY TZ SY FREQ TX TY TZ SY FREQ');
PUT EDIT ((SKIP(2),A,A,A); PUT SKIP(2);
PUT EDIT ((RESULT(I) DO I = 1 TO #XYZ))(4 F(3),6 B(1),F(4,0));
FREE STORE;
RETURN;
END PART5;

```

```

* PROCESS('ATR,XREF,NOSTMT,OPT=02');
/* CHOOSE THE MOST FREQUENT VALUE OF TX, TY, AND TZ */
PART6: PROCEDURE (IACR, IDWN, ILAY);
/*
THIS SUBROUTINE CHECKS THROUGH ALL OF THE PEAKS MAPPED INTO EACH
OTHER TO FIND THE HIGHEST SYMMETRY ELEMENT INTO WHICH ALL THE
LOWER SYMMETRY ELEMENTS HAVE BEEN MAPPED, WHICH HIGHER SYMMETRY
ELEMENT ALSO HAS THE HIGHEST FREQUENCY. IF THIS SYMMETRY ELEMENT
IS SUCH THAT ALL OF THE OTHER SYMMETRY ELEMENT TYPES HAVE BEEN
MAPPED INTO IT, THE PROGRAM SETS THE APPROPRIATE VALUES OF TX, TY,
& TZ AND EXITS. IF THIS LEAVES ANY ONE OF TX, TY, OR TZ UNDETER-
MINED, IT IS SET TO ZERO, AS THE ORIGIN IN THAT DIRECTION MAY BE
SET TO ANY VALUE. IF THE SYMMETRY ELEMENTS DETERMINE ALL THREE
OF TX, TY, TZ BUT DO NOT OVERLAP, SUCH AS TX.TZ AND TY, THE HIGHEST

```

FREQUENCY OF EACH IS USED TO DETERMINE THE POSITION OF THE ORIGIN. -P6-0150
 IF THE SYMMETRY ELEMENTS OVERLAP, SUCH AS TX.TY, TY.TZ, AND TX.TZ, -P6-0160
 THEN THE DIFFERENT SYMMETRY TYPES ARE SEPARATED INTO THREE ARRAYS, -P6-0170
 ONE FOR TX.TY, ONE FOR TY.TZ, AND ONE FOR TX.TZ, SORTED BY DECREASING -P6-0180
 FREQUENCY. THE THREE ARRAYS ARE THEN MERGED, IN THE FOLLOWING MANNER: -P6-0190
 LET TX1.TY1, TY2.TZ2, & TX3.TZ3 BE THE THREE DOUBLES. -P6-0200
 THEN, IF TX1=TX3 & TY1=TY2 & TZ2=TZ3, THE TRIPLE TX1.TY2.TZ3 IS -P6-0210
 THEN SAVED WITH THE SUM OF THE THREE FREQUENCIES. THE TRIPLE -P6-0220
 WITH THE HIGHEST FREQUENCY SUM IS THEN USED AS THE ORIGIN. -P6-0230

```

                                */ -P6-0240
DECLARE   DBG                   EXTERNAL BIT (1); -P6-0250
DECLARE   (ION(7),SGNL,NCNT)    BIT (1) EXTERNAL; -P6-0260
DECLARE   (IA8,ID8,IL8,#XYZ)   FIXED BINARY (15) EXTERNAL; -P6-0270
DECLARE   1 RESULT (#XYZ)      CONTROLLED EXTERNAL, -P6-0280
                                2 (RX,RY,RZ,RS) FIXED BINARY (15), -P6-0290
                                2 (BX,BY,BXY,BZ,BXZ,BYZ) BIT (1), -P6-0300
                                2 CK          FLOAT BINARY; -P6-0310
DECLARE   (CKR (7), CKDB)      BIT (6); -P6-0320
DECLARE   CKOK (7)            FLOAT BINARY; -P6-0330
DECLARE   JOK (7)             FIXED BINARY (15); -P6-0340
DECLARE   1 S2XY3 (IAD8)      CONTROLLED, -P6-0350
                                2 (X3, Y3)   FIXED BINARY (15), -P6-0360
                                2 OK3        FLOAT BINARY; -P6-0370
DECLARE   1 S2XZ5 (IAL8)      CONTROLLED, -P6-0380
                                2 (X5, Z5)   FIXED BINARY (15), -P6-0390
                                2 OK5        FLOAT BINARY; -P6-0400
DECLARE   1 S2YZ6 (IDL8)      CONTROLLED, -P6-0410
                                2 (Y6, Z6)   FIXED BINARY (15), -P6-0420
                                2 OK6        FLOAT BINARY; -P6-0430
DECLARE   (J3,K3,L5,J5,K6,L6) FIXED BINARY (15); -P6-0440
DECLARE   CHR                  CHARACTER (1); -P6-0450
DECLARE   (IFX, IFY, IFZ)     FIXED BINARY (15) EXTERNAL; -P6-0460
DECLARE   FOK                  FLOAT BINARY; -P6-0470
DECLARE   1 FXYZ (#OK)        CONTROLLED EXTERNAL, -P6-0480
                                2 (XR, YR, ZR, SR) FIXED BINARY (15), -P6-0490
                                2 BSTRG      BIT (6), -P6-0500
                                2 GOK        FLOAT BINARY; -P6-0510
DECLARE   #OK                  FIXED BINARY EXTERNAL; -P6-0520
ON SUBSCRIPTRANGE SNAP BEGIN; PUT DATA -P6-0530
(#OK,INDX,II,J,JRS,IRS,JFNL,I3,I3,I6,J3,J5,J6,I,L,K,I356); -P6-0540
                                EXIT; -P6-0550
                                END; -P6-0560

```

/*

"CKR" HOLDS BIT STRINGS TO BE CHECKED. FOR EXAMPLE IF THERE -P6-0570
 ARE THE FOLLOWING SYMMETRY ELEMENTS TY, TX.TZ, TX.TY.TZ, -P6-0580
 AS IN P21/C, THEN ONE WOULD HAVE ION(1), ION(3), ION(4), ION(6) -P6-0590
 =0 AND ION(2), ION(5), ION(7) = 1. PARTS SHOULD HAVE MAPPED -P6-0600
 TY INTO TX.TY.TZ AND TX.TZ INTO TX.TY.TZ, AND WOULD HAVE LEFT -P6-0610
 A RECORD OF SUCH MAPPING. IF, FOR A PARTICULAR TRIPLE OF -P6-0620
 TX.TY.TZ THERE IS NO INDICATION OF BOTH TY AND TX.TZ BEING -P6-0630
 MAPPED IN, THEN THAT TRIPLE IS ASSUMED TO BE FALSE. -P6-0640

```

P6-065:0
P6-066:0
P6-067:0
P6-068:0
P6-069:0
P6-070:0
P6-071:0
P6-072:0
P6-073:0
P6-074:0
P6-075:0
P6-076:0
P6-077:0
P6-078:0
P6-079:0
P6-080:0
P6-081:0
P6-082:0
P6-083:0
P6-084:0
P6-085:0
P6-086:0
P6-087:0
P6-088:0
P6-089:0
P6-090:0
P6-091:0
P6-092:0
P6-093:0
P6-094:0
P6-095:0
P6-096:0
P6-097:0
P6-098:0
P6-099:0
P6-100:0
P6-101:0
P6-102:0
P6-103:0
P6-104:0
P6-105:0
P6-106:0
P6-107:0
P6-108:0
P6-109:0
P6-110:0
P6-111:0
P6-112:0
P6-113:0
P6-114:0

CKR(7) = ION(1)
CKR(6) = ION(2)
CKR(5) = ION(3)
CKR(4) = ION(4)
CKR(3) = ION(5)
CKR(2) = ION(6)
IF (DBG) THEN PUT EDIT('CKR = ',CKR) (SKIP,A,7 (B(7),X(1)));
CKOK = 0.000;
JOK = 0;
IRS = 0;
IAD8 = IA8 * ID8 * 2;
#OK = 0;
IDL8 = ID8 * IL8 * 2;
IAL8 = IA8 * IL8 * 2;
/*
DETERMINE THE HIGHEST SYMMETRY ELEMENT TO BE CONSIDERED
LUPJ:
DO J = 1 TO #XYZ BY 1;
CKDB = BX(J) || BY(J) || BXY(J) || BZ(J) || BXZ(J) || BYZ(J);
JRS = RS(J);
IF (CKDB /= CKR(JRS)) THEN DO;
  OK(J) = 0.000;
  GO TO NDJL;
  IF (OK(J) > CKOK(JRS)) THEN DO;
    CKOK(JRS) = OK(J);
    JOK(JRS) = J;
  END;
  IF (JRS = 4) THEN JRS = 3;
  IF (JRS = 3) THEN JRS = 4;
  IF (OK(J) >= IRS) THEN IRS = JRS;
  IF (OK(J) > 0.0) THEN #OK = #OK + 1;
END LUPJ;
IF (DBG) THEN DO;
  PUT EDIT('SAVED TX, TY, TZ --- BEFORE MERGING & SORTING')
  PUT EDIT(' (PAGE,A)');
  PUT EDIT(' TX TY TZ SY FREQ TX TY TZ SY FREQ');
  PUT EDIT(' TX TY TZ SY FREQ TX TY TZ SY FREQ');
  PUT EDIT(' (SKIP(2),A,A,A)');
  PUT EDIT(' (SKIP(1),DO CKOK = 1, TO #XYZ)(4 F(3),6 B(1),F(4,0));');
  PUT EDIT(' (JOK = JOK, CKOK);');
  PUT EDIT(' (SKIP,A,7 F(5),X(10),A,7 F(10,2));');
  ELSE;
BRANCH, DEPENDING ON THE TYPE OF THE HIGHEST SYMM. ELEMENT
/*
IF (IRS = 3) THEN IRS = 4;
IF (IRS = 4) THEN IRS = 3;
JFNL = JOK(IRS);
IFX = RX(JFNL);
IFY = RY(JFNL);
/*

```

```

IFZ = RZ(JFNL);
FOK = OK(JFNL);
IF ((IRS=7) THEN GO TO CMP7;
IF ((IRS=6) & (~ION(5)) & (~ION(3))) THEN GO TO CMP6;
IF ((IRS=5) & (~ION(6)) & (~ION(3))) THEN GO TO CMP5;
IF ((IRS=3) & (~ION(6)) & (~ION(5))) THEN GO TO CMP3;
IF ((IRS=4) | (IRS=2) | (IRS=1)) THEN GO TO CMPL;
/*
THERE ARE THREE TWO-FOLD AXES OR TWO-FOLD SCREW AXES
ALLOCATE S2XY3, S2XZ5, S2YZ6;
X3, Y3 = 0;
OK3 = 0.000;
X5, Z5 = 0;
OK5 = 0.000;
Y6, Z6 = 0;
OK6 = 0.000;
I3, I5, I6 = 1;
J3 = JOK(3);
J5 = JOK(5);
J6 = JOK(6);
I356 = 3;
K356, L356 = 0;
OK3, OK5, OK6 = 0.000;
A3: IF (I3 > (IAC8)) THEN GO TO A5;
IF (J3 = 0) THEN GO TO A5;
X3(I3) = RX(J3);
Y3(I3) = RY(J3);
OK3(I3) = OK(J3);
OK(J3) = 0.000;
A5: IF (I5 > (IAL8)) THEN GO TO A6;
IF (J5 = 0) THEN GO TO A6;
X5(I5) = RX(J5);
Z5(I5) = RZ(J5);
OK5(I5) = OK(J5);
OK(J5) = 0.000;
A6: IF (I6 > (IDL8)) THEN GO TO Z356;
IF (J6 = 0) THEN GO TO Z356;
Y6(I6) = RY(J6);
Z6(I6) = RZ(J6);
OK6(I6) = OK(J6);
OK(J6) = 0.000;
/*
PLACE ALL OF THE TWO-FOLDS IN ARRAYS IN DESCENDING ORDER
Z356: K356 = L356;
L356 = I356;
I356 = I3 + I5 + I6;
IF (K356=I356) THEN GO TO PKAL;
IF (DBG) THEN PUT EDIT (I356) (F(6));

```

```

-P6-1150
-P6-1160
ELSE; -P6-1170
ELSE; -P6-1180
ELSE; -P6-1190
ELSE; -P6-1200
ELSE; -P6-1210
-P6-1220
-P6-1230
*/ -P6-1240
-P6-1250
-P6-1260
-P6-1270
-P6-1280
-P6-1290
-P6-1300
-P6-1310
-P6-1320
-P6-1330
-P6-1340
-P6-1350
-P6-1360
-P6-1370
-P6-1380
ELSE; -P6-1390
ELSE; -P6-1400
-P6-1410
-P6-1420
-P6-1430
-P6-1440
ELSE; -P6-1450
ELSE; -P6-1460
-P6-1470
-P6-1480
-P6-1490
-P6-1500
ELSE; -P6-1510
ELSE; -P6-1520
-P6-1530
-P6-1540
-P6-1550
-P6-1560
-P6-1570
-P6-1580
*/ -P6-1590
-P6-1600
-P6-1610
-P6-1620
ELSE; -P6-1630
ELSE; -P6-1640

```



```

J3, J5, J6 = 0;
B3, B5, B6 = 0.001;
IF (I356 > #XYZ) THEN GO TO PKAL;
DO I = 1 TO #XYZ BY 1;
OK356 = OK(I);
J356 = RS(I);
IF ((OK356 > B3) & (J356 = 3)) THEN DO;
    B3 = OK356;
    J3 = I;
    END;
ELSE;
IF ((OK356 > B5) & (J356 = 5)) THEN DO;
    B5 = OK356;
    J5 = I;
    END;
ELSE;
IF ((OK356 > B6) & (J356 = 6)) THEN DO;
    B6 = OK356;
    J6 = I;
    END;
ELSE;
END DLUP;
IF (J3 = 0) THEN I3 = I3 + 1;
IF (J5 = 0) THEN I5 = I5 + 1;
IF (J6 = 0) THEN I6 = I6 + 1;
IF ((I3 > (IAL8)) & (I5 > (IAL8)) & (I6 > (IDL8)))
    THEN GO TO PKAL; ELSE GO TO A3;
/*
FIND THE MOST FREQUENT AND CONSISTANT TX.TY.TZ
*/
PKAL:
I356 = 0;
OK = 0.000;
IF (DBG) THEN DO;
PUT EDIT ('SORTED TX.TY, TY.TZ, TX.TZ -- PART 6')
(SKIP(4),A);
PUT EDIT (' TX TY TZ SY      FREQ TX TY TZ SY      FREQ',
' TX TY TZ SY      FREQ TX TY TZ SY      FREQ',
' TX TY TZ SY      FREQ TX TY TZ SY      FREQ')
(SKIP(2),A,A,A); PUT SKIP(2);
PUT EDIT ((S2XY3(I) DO I = 1 TO IAD8))
(2 F(3),X(9),F(7,0));
PUT EDIT ((S2XZ5(I) DO I = 1 TO IAL8))
(F(3),X(3),F(3),X(6),F(7,0));
PUT EDIT ((S2YZ6(I) DO I = 1 TO IDL8))
(X(3),2 F(3),X(6),F(7,0));
END;
ELSE;
LP6: DO L = 1 TO IDL8 BY 1;
IF (OK6(L) = 0.000) THEN GO TO FNL2S;
ELSE;
K6 = Y6(L);
L6 = Z6(L);
LP5: DO K = 1 TO IAL8 BY 1;
IF (OK5(K) = 0.000) THEN GO TO NDL5;
ELSE;
J5 = X5(K);
L5 = Z5(K);
LP3: DO J = 1 TO IAD8 BY 1;
IF (OK3(J) = 0.000) THEN GO TO NDL3;
ELSE;

```

```

-P6-1650
-P6-1660
-P6-1670
-P6-1680
-P6-1690
-P6-1700
-P6-1710
-P6-1720
-P6-1730
-P6-1740
-P6-1750
-P6-1760
-P6-1770
-P6-1780
-P6-1790
-P6-1800
-P6-1810
-P6-1820
-P6-1830
-P6-1840
-P6-1850
-P6-1860
-P6-1870
-P6-1880
-P6-1890
-P6-1900
-P6-1910
-P6-1920
-P6-1930
-P6-1940
-P6-1950
-P6-1960
-P6-1970
-P6-1980
-P6-1990
-P6-2000
-P6-2010
-P6-2020
-P6-2030
-P6-2040
-P6-2050
-P6-2060
-P6-2070
-P6-2080
-P6-2090
-P6-2100
-P6-2110
-P6-2120
-P6-2130
-P6-2140

```

```

J3 = X3(J);
K3 = Y3(J);
IF ((J3=J5)&(K3=K6) & (L5=L6)) THEN GOOD: DO;
    I356 = I356 + 1;
    IF (I356 > #XYZ) THEN GO TO FNL2S; ELSE;
    RX(I356) = J3;
    RY(I356) = K3;
    RZ(I356) = L5;
    RS(I356) = 7;
    OK(I356) = OK6(L) + OK5(K) + OK3(J);
NDL3: END LP3;
NDL5: END LP5;
END LP6;
FNL2S: IF (DBG) THEN DO;
    PUT EDIT ('MERGED TX.TY, TY.TZ, TX.TZ -- PART 6')
    (SKIP(4),A);
    PUT EDIT (' TX TY TZ SY      FREQ TX TY TZ SY      FREQ',
    ' TX TY TZ SY      FREQ TX TY TZ SY      FREQ',
    ' TX TY TZ SY      FREQ TX TY TZ SY      FREQ');
    (SKIP(2),A,A,A); PUT SKIP(2);
    PUT EDIT ((RX(I),RY(I),RZ(I),RS(I),OK(I)) DC I = 1 TO #XYZ)
    (3 F(3),F(2),F(1),0));
    END; ELSE;
FOK = 0.000;
FLUP: DO M = 1 TO #XYZ BY 1;
    IF (OK(M) > FOK) THEN DO;
        MF = M;
        FOK = OK(M); END; ELSE;
    END FLUP;
    IFX = RX(MF);
    IFY = RY(MF);
    IFZ = RZ(MF);
    GO TO WXYZ;
/*
    THERE IS AN INVERSION CENTER
CMP7: PUT EDIT ('THE HIGHEST SYMMETRY ELEMENT IS AN INVERSION.')
    (SKIP(4),A);
    GO TO WXYZ;
/*
    THE HIGHEST SYMMETRY ELEMENT IS A TWO-FOLD OR SCREW
CMP6: CHR = 'X';
    IF (JOK(1) /= 0) THEN DO;
        IFX = RX(JOK(1));
        FOK = FOK + OK(JOK(1));
        GO TO P2G; END; ELSE;
    IFX = 0;
    GO TO P2B;
CMP5: CHR = 'Y';

```

```

-P6-2150
-P6-2160
-P6-2170
-P6-2180
-P6-2190
-P6-2200
-P6-2210
-P6-2220
-P6-2230
-P6-2240
-P6-2250
-P6-2260
-P6-2270
-P6-2280
-P6-2290
-P6-2300
-P6-2310
-P6-2320
-P6-2330
-P6-2340
-P6-2350
-P6-2360
-P6-2370
-P6-2380
-P6-2390
-P6-2400
-P6-2410
-P6-2420
-P6-2430
-P6-2440
-P6-2450
-P6-2460
-P6-2470
-P6-2480
-P6-2490
-P6-2500
-P6-2510
-P6-2520
-P6-2530
-P6-2540
-P6-2550
-P6-2560
-P6-2570
-P6-2580
-P6-2590
-P6-2600
-P6-2610
-P6-2620
-P6-2630
-P6-2640

```

```

IF (JOK(2) /= 0) THEN DO;                                     -P6-2650
  IFY = RY(JOK(2));                                         -P6-2660
  FCK = FOK + OK(JOK(2));                                   -P6-2670
  GO TO P2G; END;                                           ELSE; -P6-2680
IFY = 0;                                                    -P6-2690
GO TO P2B;                                                  -P6-2700
CMP3: CHR = 'Z';                                           -P6-2710
IF (JOK(4) /= 0) THEN DO;                                   -P6-2720
  IFZ = RZ(JOK(4));                                         -P6-2730
  FOK = FCK + OK(JOK(4));                                   -P6-2740
  GO TO P2G; END;                                           ELSE; -P6-2750
IFZ = 0;                                                    -P6-2760
P2B: PUT EDIT (' THE HIGHEST SYMMETRY ELEMENT IS AN AXIS IN ',CHR, -P6-2770
  'UNABLE TO DETERMINE T',CHR,'. THUS, T',CHR, -P6-2780
  ' SET EQUAL TO ZERO. '); -P6-2790
  (SKIP(4),X(10),A,A(1),SKIP(1),X(20),3 (A,A(1))); -P6-2800
GO TO WXYZ;                                                 -P6-2810
P2G: PUT EDIT (' THE HIGHEST SYMMETRY ELEMENT IS AN AXIS IN ',CHR, -P6-2820
  'HOWEVER, THERE IS A PLANE NORMAL TO ',CHR) -P6-2830
  (SKIP(4),X(10),A,A(1),SKIP(1),X(20),A,A(1)); -P6-2840
GO TO WXYZ;                                                 -P6-2850
/*                                                         -P6-2860
THERE IS ONLY A MIRROR OR GLIDE PLANE NORMAL TO ONE AXIS -P6-2870
*/                                                         -P6-2880
CMLP: PUT EDIT ('THERE IS ONLY A PLANE NORMAL TO ONE AXIS.', -P6-2890
  'THE T',S IN THE OTHER DIRECTIONS ARE SET =0. '); -P6-2900
  (SKIP(4),X(10),A,SKIP(1),X(20),A); -P6-2910
IFX, IFY, IFZ = 0;                                         -P6-2920
IF (IRS = 4) THEN IFZ = RZ(JFNL); ELSE; -P6-2930
IF (IRS = 2) THEN IFY = RY(JFNL); ELSE; -P6-2940
IF (IRS = 1) THEN IFX = RX(JFNL); ELSE; -P6-2950
WXYZ: PUT EDIT ('***** TX =',IFX,'TY =',IFY,'TZ =',IFZ) -P6-2960
  (SKIP(2),3 (A,F(5),X(5))); -P6-2970
FREE S2YZ6, S2XY3, S2XZ5; -P6-2980
ALLOCATE FXYZ; -P6-2990
INDX = 0; -P6-3000
PUT EDIT ('SAVED TRIPLES, DOUBLES, AND SINGLES') (PAGE,A); -P6-3010
PUT EDIT (' TX TY TZ SY FREQ TX TY TZ SY FREQ', -P6-3020
  ' TX TY TZ SY FREQ TX TY TZ SY FREQ', -P6-3030
  ' TX TY TZ SY FREQ TX TY TZ SY FREQ'); -P6-3040
  (SKIP(2),A,A,A); PUT SKIP(2); -P6-3050
IILP: DO II = 1 TO #XYZ BY 1; -P6-3060
IF (CK(II) > 1) THEN GD: DO; -P6-3070
INDX = INDX + 1; -P6-3080
XR(INDX) = RX(II); -P6-3090
YR(INDX) = RY(II); -P6-3100
ZR(INDX) = RZ(II); -P6-3110
SR(INDX) = RS(II); -P6-3120
GOK(INDX) = OK(II); -P6-3130
BSTRG(INDX) = BX(II) || BY(II) || BXY(II) || BZ(II) -P6-3140

```

```

                || BXZ(II) || BYZ(II);
PUT EDIT (FXYZ(INDX)) (4 F(3),B(6),F(4,0));
END GD;
FREE RESULT;
RETURN;
END PART6;

```

-P6-3150
 -P6-3160
 -P6-3170
 -P6-3180
 -P6-3190
 -P6-3200

```

* PROCESS(*ATR,XREF,NOSTMT,OPT=02*);
/* DETERMINE WHICH PEAKS ARE TO BE KEPT
PART7: PROCEDURE (IACR, IDWN, ILAY, #RTND, #SYMM);
/*
THIS SUBROUTINE MAKES USE OF THE ORIGIN TRANSLATION TX.TY.TZ AND
OF THE SYMMETRY ELEMENTS TO DETERMINE WHICH PEAKS FIT IN E.D.
SPACE. IF AT LEAST HALF OF THE SYMMETRY-RELATED PEAKS ARE PRESENT
WHEN THE ENTIRE MAP HAS BEEN SHIFTED BY TX.TY.TZ, THEN THAT SET
OF PEAKS IS OUTPUT IN THE SHIFTED COORDINATES
DECLARE (IACR, IDWN, ILAY, #RTND, #SYMM) FIXED BINARY (15);
DECLARE (IFX, IFY, IFZ) FIXED BINARY (15) EXTERNAL;
DECLARE 1 SYMMPQ (#SYMM) CONTROLLED EXTERNAL;
2 (PX, QX, PY, QY, PZ, QZ) FIXED BINARY (15);
DECLARE #OK FIXED BINARY EXTERNAL;
DECLARE 1 FXYZ (#OK) CONTROLLED EXTERNAL;
2 (XR, YR, ZR, SR) FIXED BINARY (15);
2 BSTRG BIT (6);
2 GOK FLOAT BINARY;
DECLARE 1 PEAKS (#RTND) CONTROLLED;
2 (U, V, W, VLU, X, Y, Z) FIXED BINARY;
DECLARE 1 PEAKR,
2 (RU, RV, RW, VAL, AVG) FIXED BINARY (31);
DECLARE (RETAIN, FINAL) FILE RECORD SEQUENTIAL;
DECLARE (BX, BY, BZ) BIT (1);
DECLARE DBG BIT (1) EXTERNAL;
ON SUBSCRIPTRANGE SNAP BEGIN; PUT DATA (I, J, K); EXIT; END;
DECLARE JAVG (#SYMM) CONTROLLED FIXED BINARY;
DECLARE PVALUE (16) FIXED BINARY (15);
DECLARE (L, M, N) FIXED BINARY (15);
DECLARE (KX, KY, KZ, NSY, CL(24)) FIXED BINARY (15);
DECLARE 1 FPEAK,
2 (HITE, FX, FY, FZ, #) FIXED BINARY (31);
DECLARE ONE FLOAT BINARY;
ONE = 1.0000;
CL(1), CL( 7), CL(13), CL(19) = 40;
CL(2), CL( 8), CL(14), CL(20) = 56;
CL(3), CL( 9), CL(15), CL(21) = 72;
CL(4), CL(10), CL(16), CL(22) = 88;
CL(5), CL(11), CL(17), CL(23) = 104;

```

-P7-0010
 -P7-0020
 -P7-0030
 -P7-0040
 -P7-0050
 -P7-0060
 -P7-0070
 -P7-0080
 -P7-0090
 -P7-0100
 -P7-0110
 -P7-0120
 -P7-0130
 -P7-0140
 -P7-0150
 -P7-0160
 -P7-0170
 -P7-0180
 -P7-0190
 -P7-0200
 -P7-0210
 -P7-0220
 -P7-0230
 -P7-0240
 -P7-0250
 -P7-0260
 -P7-0270
 -P7-0280
 -P7-0290
 -P7-0300
 -P7-0310
 -P7-0320
 -P7-0330
 -P7-0340
 -P7-0350
 -P7-0360
 -P7-0370
 -P7-0380
 -P7-0390
 -P7-0400

```

CL(6), CL(12), CL(18), CL(24) = 120; -P7-0410
L = ROUND (FLOAT (IACR) / 16.000, 0); -P7-0420
M = ROUND (FLOAT (IDWN) / 16.000, 0); -P7-0430
N = ROUND (FLOAT (ILAY) / 16.000, 0); -P7-0440
ISYM = MAX (#SYMM/2 +1, 1); -P7-0450
IPEAK = 0; -P7-0460
QACR = FLOAT (IACR); -P7-0470
QDWN = FLOAT (IDWN); -P7-0480
QLAY = FLOAT (ILAY); -P7-0490
ALLOCATE PEAKS; -P7-0500
ALLOCATE JAVG; -P7-0510
IF (DBG) THEN PUT EDIT ('$$$$ TX =', IFX, 'TY =', IFY, 'TZ =', -P7-0520
IFZ) (SKIP(4), 3 (A, F(5), X(5))); ELSE; -P7-0530
/* -P7-0540
READ AND STORE THE PEAKS, TRANSFORMING THEM TO E.D. COORDS. */ -P7-0550
-P7-0560
RLUP: OPEN FILE (RETAIN) INPUT; -P7-0570
DO I = 1 TO #RTND BY 1; -P7-0580
READ FILE (RETAIN) INTO (PEAKR); -P7-0590
U(I) = RU; -P7-0600
V(I) = RV; -P7-0610
W(I) = RW; -P7-0620
VLU(I) = AVG; -P7-0630
X(I) = MOD (RU - IFX, IACR); -P7-0640
Y(I) = MOD (RV - IFY, IDWN); -P7-0650
Z(I) = MOD (RW - IFZ, ILAY); -P7-0660
END RLUP; -P7-0670
CLOSE FILE (RETAIN); -P7-0680
OPEN FILE (FINAL) OUTPUT; -P7-0690
NPEAK = 0; -P7-0700
PUT EDIT ('PEAK BEING CHECKED (PART7) -- #, OR', -P7-0710
' ORIGINAL (UVW) & TRANSFORMED (XYZ) COORDS., EQUIV. P', -P7-0720
' POSITIONS (EX, EY, EZ), & # OF MATCHING PEAK (#MP)', -P7-0730
' # U V W VALUE X Y Z', -P7-0740
' EX EY EZ #MP EX EY EZ #MP EX EY EZ #MP', -P7-0750
' EX EY EZ #MP EX EY EZ #MP EX EY EZ #MP', -P7-0760
(PAGE, A, A, A, SKIP, A, A, A); -P7-0770
-P7-0780
/* -P7-0790
LOOP THROUGH ALL RETAINED PEAKS TO DETERMINE WHICH ONES ARE -P7-0800
ALLOWED BY SYMMETRY AND OUTPUTTING THE ALLOWED PEAKS. */ -P7-0810
-P7-0820
ILUP: DO I = 1 TO #RTND BY 1; -P7-0830
IF (VLU(I) < 1.00) THEN GO TO NDIL; ELSE; -P7-0840
RU = U(I); -P7-0850
RV = V(I); -P7-0860
RW = W(I); -P7-0870
VAL = VLU(I); -P7-0880
IVAL = VAL; -P7-0890
AVG = 0; -P7-0900

```

```

RX = X(I);
RY = Y(I);
RZ = Z(I);
PUT EDIT (I,RU,RV,RW,VAL,RX,RY,RZ)
      (SKIP,F(3),3 F(4),F(6),3 F(4));
/*
CREATE EQUIVALENT POSITIONS FROM SYMMETRY ELEMENTS
SLUP: DO K = 1 TO #SYMM BY 1;
      KX = MOD ((RX * PX(K)) + QX(K), IACR);
      KY = MOD ((RY * PY(K)) + QY(K), IDWN);
      KZ = MOD ((RZ * PZ(K)) + QZ(K), ILAY);
      KXI = KX + IACR;
      KYI = KY + IDWN;
      KZI = KZ + ILAY;
      NSY = CL(K);
      PUT EDIT (KX,KY,KZ) (COL(NSY), 3 F(3));
/*
LOOP THROUGH ALL PEAKS - LOOKING FOR SYMMETRY RELATED PEAKS
JLUP: DO J = 1 TO #RTND BY 1;
      IF (VLU(J) < 1.00) THEN GO TO NDJL;
      OX = MIN (ABS(KX-X(J)),ABS(KXI-X(J)));
      OY = MIN (ABS(KY-Y(J)),ABS(KYI-Y(J)));
      OZ = MIN (ABS(KZ-Z(J)),ABS(KZI-Z(J)));
      BX = (CX <=L);
      BY = (OY <=M);
      BZ = (CZ <=N);
      IF (BX & BY & BZ) THEN GO TO PNDS;
      NDJL: END JLUP;
      GO TO NDSL;
      PNDS: AVG = AVG + 1;
            JAVG(AVG) = J;
            PUT EDIT (J) (F(4));
            IVAL = IVAL + VLU(J);
      NDSL: END SLUP;
/*
OUTPUT THE GOOD PEAKS
      IF (AVG < ISYM) THEN GO TO NDIL;
      NPEAK = NPEAK + AVG + 1;
      HITE = IVAL / (AVG + 1);
      # = AVG;
      FX = RX;
      FY = RY;
      FZ = RZ;
      VLU(I) = 0;
      WRITE FILE (FINAL) FROM (FPEAK);
      IPEAK = IPEAK + 1;
LUPJ: DO J = 1 TO AVG BY 1;

```

```

-P7-0910
-P7-0920
-P7-0930
-P7-0940
-P7-0950
-P7-0960
-P7-0970
*/ -P7-0980
-P7-0990
-P7-1000
-P7-1010
-P7-1020
-P7-1030
-P7-1040
-P7-1050
-P7-1060
-P7-1070
-P7-1080
-P7-1090
*/ -P7-1100
-P7-1110
ELSE; -P7-1120
-P7-1130
-P7-1140
-P7-1150
-P7-1160
-P7-1170
-P7-1180
ELSE; -P7-1190
-P7-1200
-P7-1210
-P7-1220
-P7-1230
-P7-1240
-P7-1250
-P7-1260
-P7-1270
-P7-1280
*/ -P7-1290
ELSE; -P7-1300
-P7-1310
-P7-1320
-P7-1330
-P7-1340
-P7-1350
-P7-1360
-P7-1370
-P7-1380
-P7-1390
-P7-1400

```

```

JS = JAVG(J);
VLU(JS) = 0;
NDLJ: END LUPJ;
NDIL: END ILUP;
PUT EDIT ('# PEAKS RETAINED =',NPEAK) (SKIP(2),A,F(5));
CLOSE FILE (FINAL);
OPEN FILE (FINAL) INPUT;
PUT EDIT ('NUMBER OF INDEPENDENT PEAKS =',IPEAK)
      {SKIP(2),A,F(5)};
PUT EDIT ('INDEPENDENT PEAKS AFTER SYMMETRY CHECK',
      ' X Y Z (FOUR.) X Y Z',
      ' (FRACT.) HEIGHT #SYMM', ' ')
      (PAGE,A,SKIP,A,A,SKIP(2),A);
/*
OUTPUT PEAKS REMAINING AFTER SYMMETRY CHECK ON "ORFLS" CARDS
WRITE OUT FOUND PEAKS AND PUNCH LEAST SQUARES CARDS
LUPI: DO I = 1 TO IPEAK BY 1;
READ FILE (FINAL) INTO (FPEAK);
XFR = FLOAT (FX) / QACR;
YFR = FLOAT (FY) / QDWN;
ZFR = FLOAT (FZ) / QLAY;
PUT EDIT (FX,FY,FZ,XFR,YFR,ZFR,HITE,#)
      (SKIP,3 F(5),X(4),3 F(10,5),X(9),2 F(10));
PUT FILE (PUNCH) EDIT (HITE,ONE,ONE,XFR,YFR,ZFR)
      (SKIP,F(5),X(4),5 F(9,5));
END LUPI;
CLOSE FILE (FINAL), FILE (PUNCH);
RETURN;
END PART7;

```

```

-P7-1410
-P7-1420
-P7-1430
-P7-1440
-P7-1450
-P7-1460
-P7-1470
-P7-1480
-P7-1490
-P7-1500
-P7-1510
-P7-1520
-P7-1530
-P7-1540
-P7-1550
-P7-1560
-P7-1570
-P7-1580
-P7-1590
-P7-1600
-P7-1610
-P7-1620
-P7-1630
-P7-1640
-P7-1650
-P7-1660
-P7-1670
-P7-1680
-P7-1690
-P7-1700

```

```

//LKED.SYSLMOD DD DSNAME=PROG,CRYST,
// UNIT=DISK,VOLUME=SER=PROGPK,CISP=(OLD,KEEP)
//LKED.SYSIN DD *
OVERLAY ALPHA
INSERT TM_DT
OVERLAY ALPHA
INSERT PART1
OVERLAY ALPHA
INSERT PART2
OVERLAY ALPHA
INSERT IHESRTA
OVERLAY ALPHA
INSERT PART3
OVERLAY ALPHA
INSERT PART4
OVERLAY ALPHA

```

```

JCL-0060
JCL-0070
JCL-0080
OVLY0010
OVLY0020
OVLY0030
OVLY0040
OVLY0050
OVLY0060
OVLY0070
OVLY0080
OVLY0090
OVLY0100
OVLY0110
OVLY0120
OVLY0130

```

INSERT PART5
OVERLAY ALPHA
INSERT PART6
OVERLAY ALPHA
INSERT PART7
NAME ALOP2(R)

OVLY0140
OVLY0150
OVLY0160
OVLY0170
OVLY0180
JCL-0090

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